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### Flight Experimentation with Magnetic Attitude Control System of SiriusSat-1&2 Nanosatellites

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#### Content

- SiriusSat-1&2 details
- On-flight sensors calibration
- Attitude and magnetometer bias estimation
- Algorithms testing results
- Conclusions

### Nanosatellites SiriusSat-1&2

#### • SiriusSat-1&2

- assembled by school students in a collaboration with SPUTNIX specialists
- educational and space weather monitoring 1U CubeSats

#### Attitude control system:

active magnetic:
 air core magnetorquers inbuilt in solar panels

#### • Attitude sensors:

- o magnetometer
- o angular velocity sensor
- Inertia tensor and mass:

$$J = \begin{bmatrix} 6.9 & 0.3 & 0 \\ 0.3 & 6.9 & 0 \\ 0 & 0 & 2.9 \end{bmatrix} \cdot 10^{-3} \text{kg} \cdot \text{m}^2; \quad m = 1.45 \text{ kg}$$
Magnetic Attitude Control System of SiriusSat-1&2



Photo of the SiriusSat-1&2

### **ACS** parameters

- The SiriusSats satellites consist of:
  - main stack of electronic devices
  - an assembly frame
  - solar panels
- The on-board computer module SXC-MB-04 is contains the following set of devices:
  - slot for the Raspberry-Pi CM3 processor
  - power supply system
  - angular velocity sensor and magnetometer
  - control unit for magnetorquers





Solar panels and inbuilt air core magnetic coils



. On-board computer SXC-MB-04



### The launch 15.08.2018

The direction of the SiruisSat-1&2 launch from ISS



Cosmonaut manual hand launch





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### Magnetometer calibration

• Magnetometer measurement model:

 $\mathbf{B}_{meas} = \mathbf{A}\mathbf{B}_{orb} + \Delta\mathbf{B} + \delta\mathbf{B}$ 

 Comparing the magnitude with IGRF geomagnetic field model value the magnetometer bias obtained



Geomagnetic field calculated using IGRF and magnetometer measurements without bias





# Attitude motion reconstruction technique

Motion equations

 $\mathbf{J}\dot{\mathbf{\Omega}} + \mathbf{\Omega} \times \mathbf{J}\mathbf{\Omega} = \mathbf{M}_{mag} + \mathbf{M}_{grav}$ 

$$\dot{\Lambda} = \frac{1}{2} \mathbf{C} \Lambda \qquad \Lambda = (\mathbf{q}, q_0)$$

Initial conditions vector

$$\boldsymbol{\xi} = \left[ q_1 \, (t=0), q_2 \, (t=0), q_3 \, (t=0), \omega_1 \, (t=0), \omega_2 \, (t=0), \omega_3 \, (t=0) \right]^T$$

The problem of the vector of initial conditions determination reduces to the problem of the following function minimization  $\Phi(\xi) = \sum_{k=1}^{N} \left( \left| \tilde{\mathbf{b}}_{model}^{k} - \mathbf{b}_{meas}^{k} \right| \right)^{2}$ 

 $\mathbf{b}_{meas}^{i}$  is the unit vector along the geomagnetic field calculated using measurements after excluding the constant bias

 $\tilde{\mathbf{b}}^{i}_{\text{mod}el}$  is the unit vector along the geomagnetic field calculated IGRF model

Measurements model

 $\mathbf{B}_{meas} = \mathbf{A}\mathbf{B}_{o} + \mathbf{B}_{bias}$ 

#### Measurements processing results

- Using magnetometer measurements the attitude motion is reconstructed
- Angular velocity sensor measurements is shifted relative to estimated angular velocity
- The sensor bias is







Measured and predicted unit vector along the geomagnetic field



Attitude guaternion

Magnetic Attitude Control System of SiriusSat-1&2



#### Magnetic control algorithms

• Magnetic three-axis attitude control to be tested

 $\mathbf{m} = -k_{\omega}\mathbf{B} \times \mathbf{\Omega} - k_{a}\mathbf{B} \times \mathbf{S}$ 

- Real-time attitude determination is necessary
- Magnetometer bias as well as angular velocity sensor bias are changing due to onboard magnetic sources
- Extended Kalman filter using magnetometer measurements is applied to the problem
- Magnetometer bias is included to the state vector

State vector of the system

$$\mathbf{x} = \left[ \mathbf{q}, \, \mathbf{\Omega}, \, \Delta \mathbf{B} \right]^T$$

Linearized motion equations

$$\delta \dot{\mathbf{x}}(t) = \mathbf{F}(t) \delta \mathbf{x}(t)$$
Dynamics matrix
$$= \begin{pmatrix} -\mathbf{W}_{\Omega} & \frac{1}{2}\mathbf{E} & \mathbf{0}_{3x3} \\ \mathbf{J}^{-1}\mathbf{F}_{qw} & \mathbf{J}^{-1}(\mathbf{F}_{gir}^{\Omega} - \mathbf{W}_{\mathbf{A}\mathbf{\omega}_{orb}}\mathbf{J}) & \mathbf{0}_{3x3} \\ \mathbf{0}_{3x3} & \mathbf{0}_{3x3} & \mathbf{0}_{3x3} \end{pmatrix}$$

F

Measurement model

 $\mathbf{z} = \mathbf{A}\mathbf{B}_{orb} + \Delta\mathbf{B} + \mathbf{\eta}_V,$ 

Linearized measurement model

$$\delta \mathbf{z} = -2\mathbf{W}_{\delta \mathbf{q}}\hat{\mathbf{B}} = -2\mathbf{W}_{\hat{\mathbf{B}}}\delta \mathbf{q}$$

Measurement matrix

$$\mathbf{H} = \begin{bmatrix} -2\mathbf{W}_{\hat{\mathbf{B}}} & \mathbf{0}_{3x3} & \mathbf{E}_{3x3} \end{bmatrix}$$

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#### **EKF Testing Using Engineering Model**

- Implemented EKF using magnetometer measurements obtained 06.08.19 is tested
- State vector estimations are converged to the close to real values
- Magnetometer bias is estimated with 1000 nT accuracy
- The attitude motrion estimation accuracy is about 3 deg
- This accuracy is enough for coarse three-axis attitude control



120

140

160

140



#### Conclusions

- Results of the angular motion analysis using the telemetry data are discussed
- The algorithm is proposed for the attitude motion and magnetometer bias estimation in real time
- The algorithm is tested using the hardware-in-the-loop technique
- Real flight data was successfully processed by the onboard computer identical to the one installed on SiriusSat satellites
- The relevant software is currently uploaded via the UHF antenna

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## Thank you for attention!

Our web-site: http://keldysh.ru/microsatellites/eng/



