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Effect of reaction wheels disbalances on the spacecraft stabilization accuracy

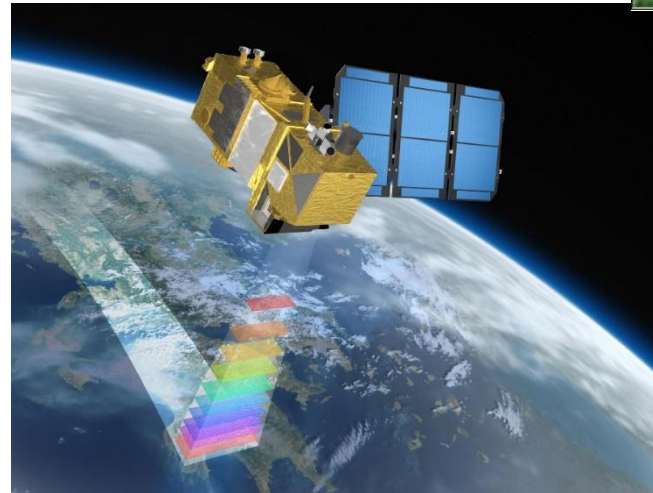
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Introduction

Most types of mission require attitude control

- Solar panels pointing for battery recharging
- Communication antennas pointing
- Intersatellite communication
- Payload requirements

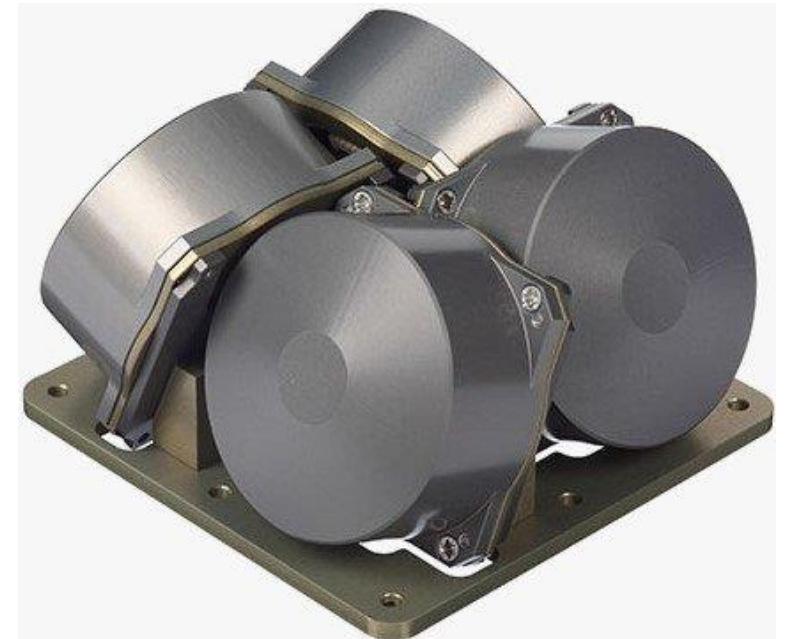


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Introduction

Several types of actuators:

- Magnetorquers
- Reaction wheels/CMGs
- Thrusters





Gyroscopic attitude control

Pros:

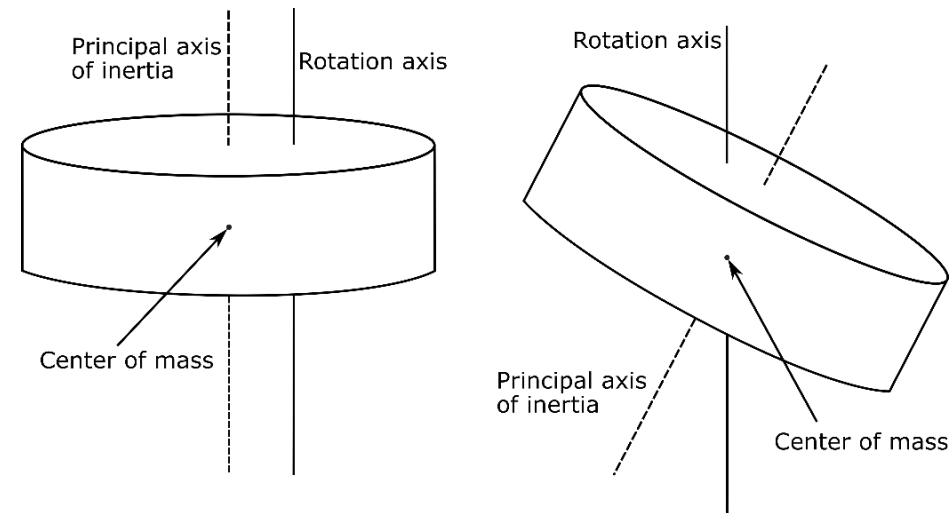
- Provide nice pointing accuracy
- Fast maneuvers

Cons:

- Saturation (can be solved by magnetorquers at LEO)
- Vibration

Why there is a problem?

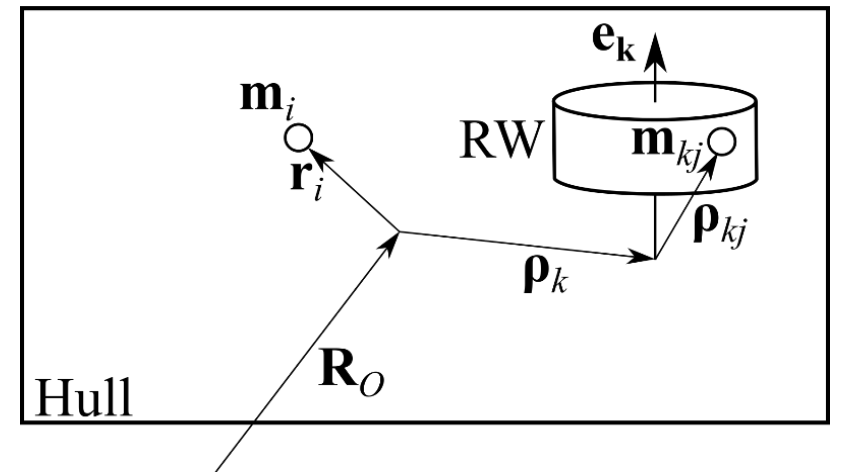
- Non-ideal balancing leads to vibration
- Two types of them: static and dynamic imbalances



What do we need?

- First of all – model of motion
- We use general equation of dynamics
- There are $6 + N$ degrees of freedom (N – amount of RWs)

$$\sum_i (m_i \ddot{\mathbf{R}}_i - \mathbf{F}_i)^T \delta \mathbf{R}_i + \sum_k \sum_j (m_{kj} \ddot{\mathbf{R}}_{kj} - \mathbf{F}_{kj})^T \delta \mathbf{R}_{kj} = \sum_k M_k^{int} \delta \varphi_k$$



Model of motion

After the mathematics we got the following equations for dynamics

$$\mathbf{S} \begin{pmatrix} \dot{\mathbf{V}}_O \\ \dot{\boldsymbol{\omega}} \\ \dot{\Omega}_1 \\ \vdots \\ \dot{\Omega}_n \end{pmatrix} = \mathbf{N}$$

$$\mathbf{S} = \begin{pmatrix} m\mathbf{E}_{3 \times 3} & -\left[\sum_k m_k \boldsymbol{\rho}_{kc} \right]_{\times} & -m_1 \boldsymbol{\rho}_{1c} \times \mathbf{e}_1 & \dots & -m_n \boldsymbol{\rho}_{nc} \times \mathbf{e}_n \\ \left[\sum_k m_k \boldsymbol{\rho}_{kc} \right]_{\times} & \mathbf{J} & (\mathbf{I}_1 - m_1 [\boldsymbol{\rho}_1]_{\times} [\boldsymbol{\rho}_{1c}]_{\times}) \mathbf{e}_1 & \dots & (\mathbf{I}_n - m_n [\boldsymbol{\rho}_n]_{\times} [\boldsymbol{\rho}_{nc}]_{\times}) \mathbf{e}_n \\ -(m_1 \boldsymbol{\rho}_{1c} \times \mathbf{e}_1)^T & \mathbf{e}_1^T (\mathbf{I}_1 - m_1 [\boldsymbol{\rho}_{1c}]_{\times} [\boldsymbol{\rho}_1]_{\times}) & I_1 & 0 & 0 \\ \vdots & \vdots & 0 & \ddots & 0 \\ -(m_n \boldsymbol{\rho}_{nc} \times \mathbf{e}_n)^T & \mathbf{e}_n^T (\mathbf{I}_n - m_n [\boldsymbol{\rho}_{nc}]_{\times} [\boldsymbol{\rho}_n]_{\times}) & 0 & 0 & I_n \end{pmatrix}$$

$$\mathbf{N} = \begin{pmatrix} \mathbf{F}_s + \sum_k \mathbf{F}_k - \sum_k m_k (\boldsymbol{\omega} \times \boldsymbol{\Omega}_k) \times \boldsymbol{\rho}_{kc} - \sum_k m_k (\boldsymbol{\omega} + \boldsymbol{\Omega}_k) \times (\boldsymbol{\omega} + \boldsymbol{\Omega}_k) \times \boldsymbol{\rho}_{kc} \\ \mathbf{N}_{\boldsymbol{\omega}} \\ M_1^{int} + \mathbf{e}_1^T \mathbf{M}_1 - \mathbf{e}_1^T (m_1 \boldsymbol{\rho}_{1c} \times \boldsymbol{\omega} \times \boldsymbol{\omega} \times \boldsymbol{\rho}_1 + \mathbf{I}_1 (\boldsymbol{\omega} \times \boldsymbol{\Omega}_1) + \boldsymbol{\omega} \times \mathbf{I}_1 (\boldsymbol{\omega} + \boldsymbol{\Omega}_1)) \\ \vdots \\ M_n^{int} + \mathbf{e}_n^T \mathbf{M}_n - \mathbf{e}_n^T (m_n \boldsymbol{\rho}_{nc} \times \boldsymbol{\omega} \times \boldsymbol{\omega} \times \boldsymbol{\rho}_n + \mathbf{I}_n (\boldsymbol{\omega} \times \boldsymbol{\Omega}_n) + \boldsymbol{\omega} \times \mathbf{I}_n (\boldsymbol{\omega} + \boldsymbol{\Omega}_n)) \end{pmatrix}$$

These equations are verified using momentum, angular momentum and energy conservation laws



What are the problems?

- It requires very small time steps
- Calculation burden might be unacceptable for Monte-Carlo simulation
- We need some estimation of the obtained accuracy, at least in the most common modes of attitude motion
- We consider inertial stabilization and standard Lyapunov-based controller

$$\mathbf{M}_{ctrl} = -k_{\omega} \boldsymbol{\omega} - k_q \mathbf{q} + \boldsymbol{\omega} \times \tilde{\mathbf{J}} \boldsymbol{\omega}$$



Attitude and stabilization accuracy

- Imbalances act as a small disturbances
- Undisturbed motion is asymptotically stable
- Motion is in the vicinity of required one

$$\mathbf{Q}_{ref} = (1, 0, 0, 0), \quad \boldsymbol{\omega}_{ref} = (0, 0, 0)$$

- Two different cases: purely static and purely dynamic imbalance



Equations of motion analysis

- Main idea – looking for solution as a power series

$$\boldsymbol{\omega} = \boldsymbol{\omega}^0 + \varepsilon \boldsymbol{\omega}^1 + \dots$$

$$\boldsymbol{\Omega}_k = \boldsymbol{\Omega}_k^0 + \varepsilon \boldsymbol{\Omega}_k^1 + \dots = \mathbf{e}_k \left(\Omega_k^0 + \varepsilon \Omega_k^1 + \dots \right)$$

$$\mathbf{q} \approx \frac{1}{2} \left(\boldsymbol{\varphi}^0 + \varepsilon \boldsymbol{\varphi}^1 + \dots \right).$$

- Epsilon here is the ratio between imbalance value and RW moment of inertia

Dynamic imbalance

- Zero approximation converges to zero
- Equations of first approximation give

$$\left(\tilde{\mathbf{J}} - \sum_k I_k^0 \mathbf{e}_k \mathbf{e}_k^T \right) \ddot{\boldsymbol{\varphi}}^1 + k_\omega \dot{\boldsymbol{\varphi}}^1 + \frac{k_q}{2} \boldsymbol{\varphi}^1 = \sum_k \boldsymbol{\Omega}_k^0 \times \mathbf{I}_k^1 \boldsymbol{\Omega}_k^0, \quad \boldsymbol{\Omega}_k^0 = \text{const}$$

- Right part depends only on time
- Final estimation

$$\Delta \boldsymbol{\omega} \approx \varepsilon \sum_k \boldsymbol{\Omega}_k^0 \left(-\mathbf{u}_k \sin(\alpha_k^0 + \boldsymbol{\Omega}_k^0 t) + \mathbf{v}_k \cos(\alpha_k^0 + \boldsymbol{\Omega}_k^0 t) \right)$$

- And in simplified form

$$\Delta \omega_{ik} \sim \Omega_k^0 d$$

Static imbalance

- Zero order approximation is the same
- First order approximation is

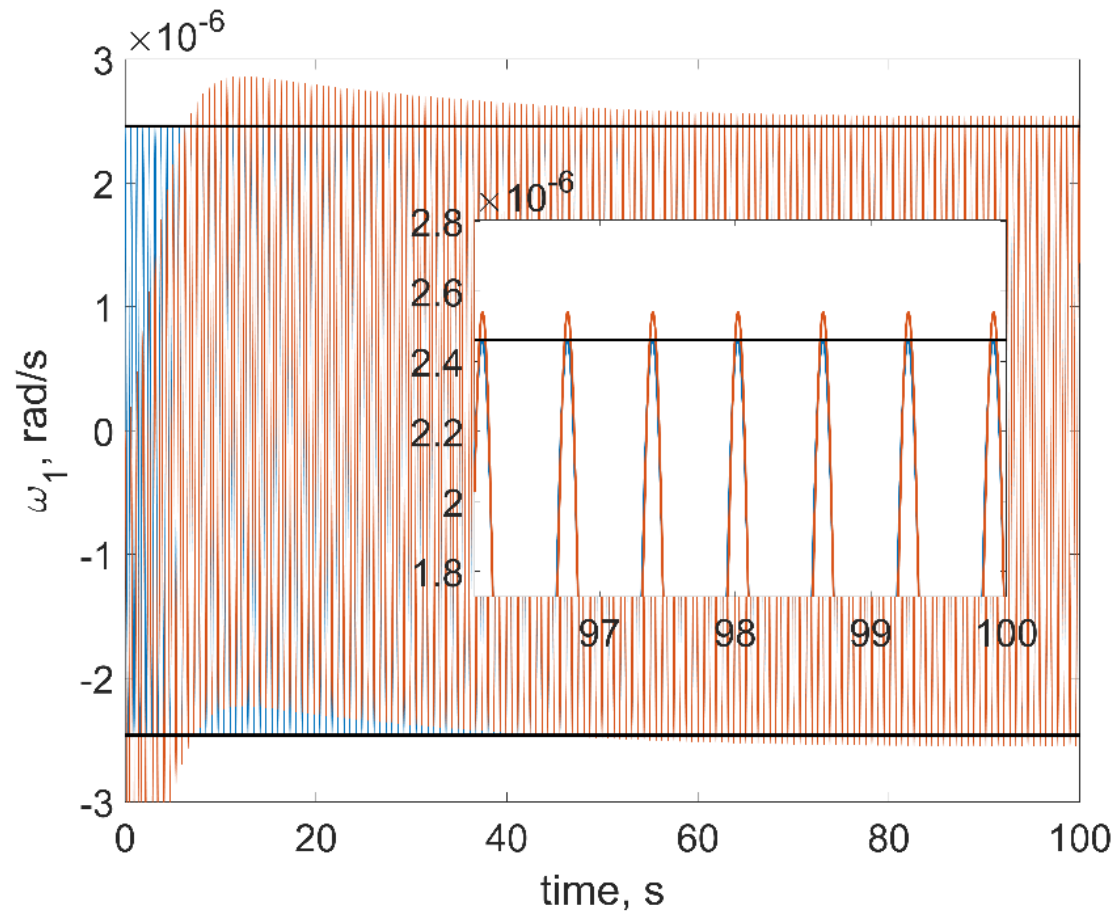
$$\left(\tilde{\mathbf{J}} - \sum_k \tilde{I}_k \mathbf{e}_k \mathbf{e}_k^T \right) \dot{\boldsymbol{\omega}}^1 + k_\omega \boldsymbol{\omega}^1 + \frac{k_q}{2} \boldsymbol{\varphi}^1 = - \sum_k m_k \boldsymbol{\rho}_k \times \boldsymbol{\Omega}_k^0 \times \boldsymbol{\Omega}_k^0 \times \delta \boldsymbol{\rho}_{kc}$$

- Again, right part depends only on time
- Solution is

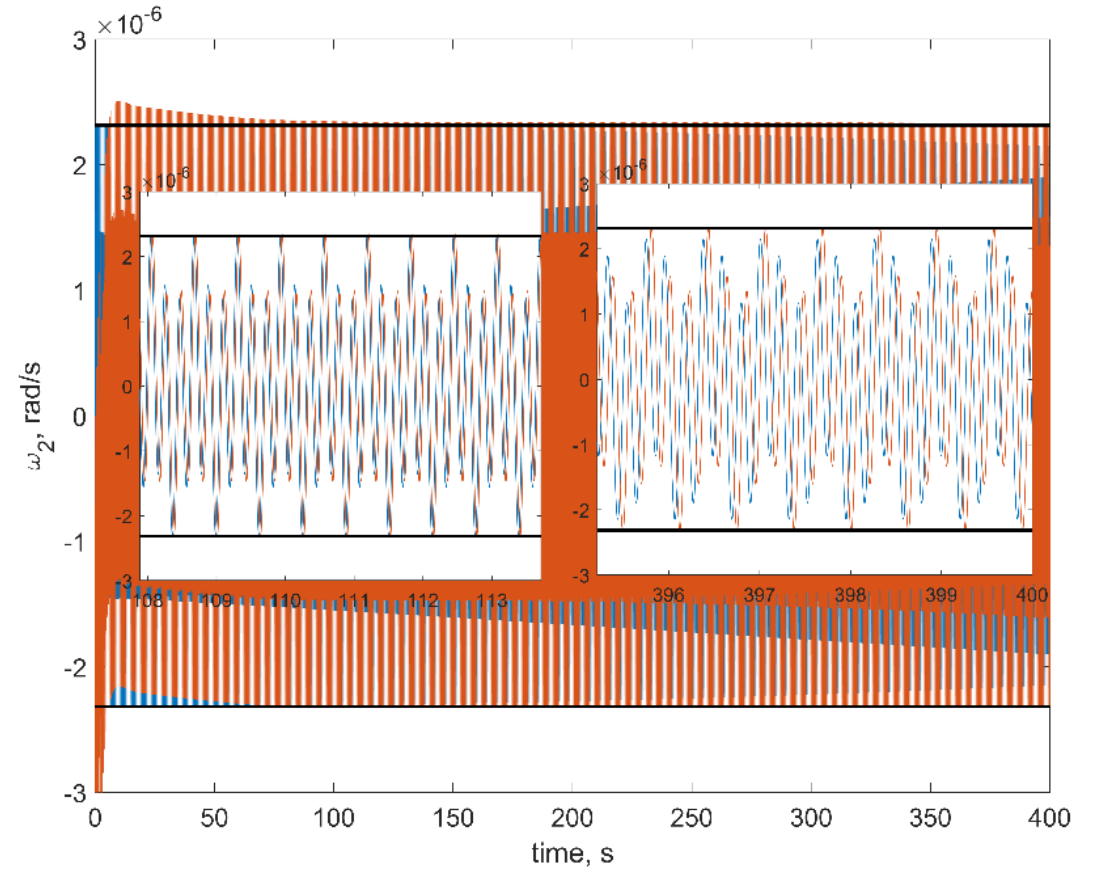
$$\Delta \boldsymbol{\omega} \approx \sum_k \rho_k \delta \rho_{kc} \boldsymbol{\Omega}_k^0 \left(-\mathbf{u}_k \sin(\alpha_k^0 + \Omega_k^0 t) + \mathbf{v}_k \cos(\alpha_k^0 + \Omega_k^0 t) \right)$$

- Depends on position of RWs: the farther they are from center of mass – the greater stabilization error

Simulation results



Static Imbalance



Dynamic Imbalance



Conclusion

- We presented a fully coupled model of motion for the satellite with imbalanced RWs
- It is verified using conservation laws for free motion
- Two cases of imbalances are considered for inertial stabilization
- Analytical estimations and numerical simulation are in a good accordance (several percent difference)

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