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Tetrahedron formation maintenance via atmospheric drag control

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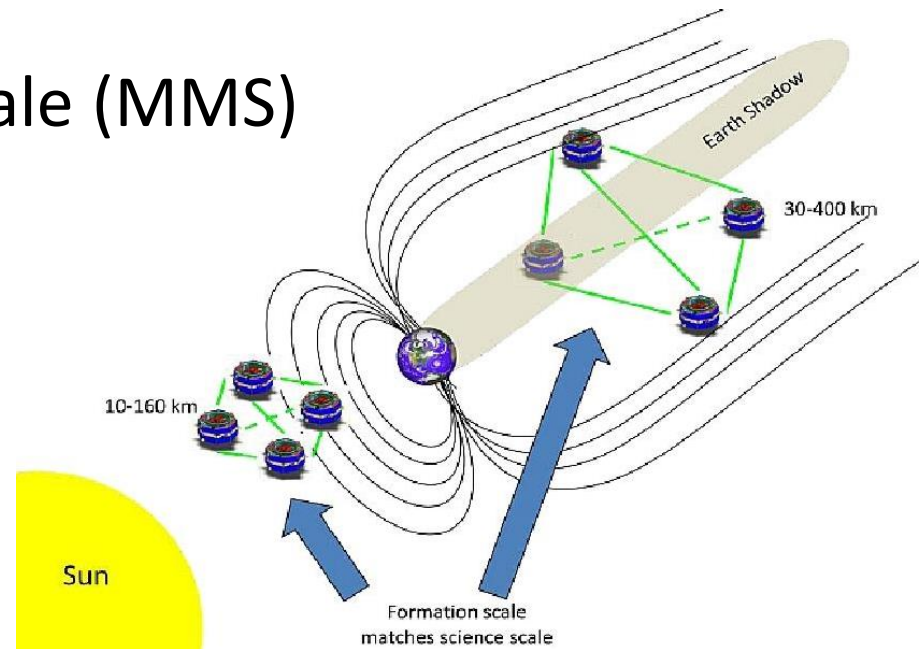
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Introduction

Missions with tetrahedral formations

- Cluster/Cluster II
- The Auroral Lites
- Magnetospheric Multiscale (MMS)



Using tetrahedral formation

- Why?
 - Physical quantities change in time and space simultaneously
 - Even in linear approximation one needs to have four measurements to have a gradient
- Magnetosphere study
- Need to maintain the tetrahedron
 - Nondegenerate for all the lifetime of the mission
 - Possibly the closest to the regular one
- It is common and convenient to describe the tetrahedron using several scalar parameters

Problem statement

- Four satellites move on close LEOs
- One is moving along circular trajectory
- Need to obtain a reference orbit in order that the volume and shape of the corresponding tetrahedron maintain over time
- Size and shape must be formalized
- Also provide a simple control algorithm for several satellites to neglect perturbations

Tetrahedral configuration

- Quality of the tetrahedron is chosen to be meaningful in geometric sense and analytically analyzable

$$Q = 12 \frac{(3 |V|)^{2/3}}{r_{12}^2 + r_{13}^2 + r_{14}^2 + r_{23}^2 + r_{24}^2 + r_{34}^2} = 12 \frac{(3 |V|)^{2/3}}{L} = 3 \frac{\sqrt[3]{\sigma_1^2 \sigma_2^2 \sigma_3^2}}{\sigma_1^2 + \sigma_2^2 + \sigma_3^2}$$

- Linearized HCW model, closed orbits described by

$$\ddot{x} - 2n\dot{y} - 3n^2 x = 0,$$

$$x_i(t) = A_i \sin \nu + B_i \cos \nu,$$

$$\ddot{y} + 2n\dot{x} = 0,$$

$$y_i(t) = 2A_i \cos \nu - 2B_i \sin \nu + C_i,$$

$$\ddot{z} + n^2 z = 0$$

$$z_i(t) = D_i \sin \nu + E_i \cos \nu,$$

- The main goal is to find such reference orbit that in passive motion in linearized model volume and quality of the tetrahedron remain constant

Quality/Volume conservation

The set of equations so that the tetrahedron does not change volume and quality in linear model



$$D_1 = aA_1 + bB_1, \quad D_2 = aA_2 + bB_2, \quad D_3 = aA_3 + bB_3,$$

$$E_1 = -bA_1 + aB_1, \quad E_2 = -bA_2 + aB_2, \quad E_3 = -bA_3 + aB_3,$$

$$3A_1B_1 + 3A_2B_2 + 3A_3B_3 - A_1B_2 - A_1B_3 - A_2B_1 - A_2B_3 - A_3B_1 - A_3B_2 = 0,$$

$$3(B_1^2 + B_2^2 + B_3^2 - A_1^2 - A_2^2 - A_3^2) + 2(A_1A_2 + A_1A_3 + A_2A_3 - B_1B_2 - B_1B_3 - B_2B_3) = 0,$$

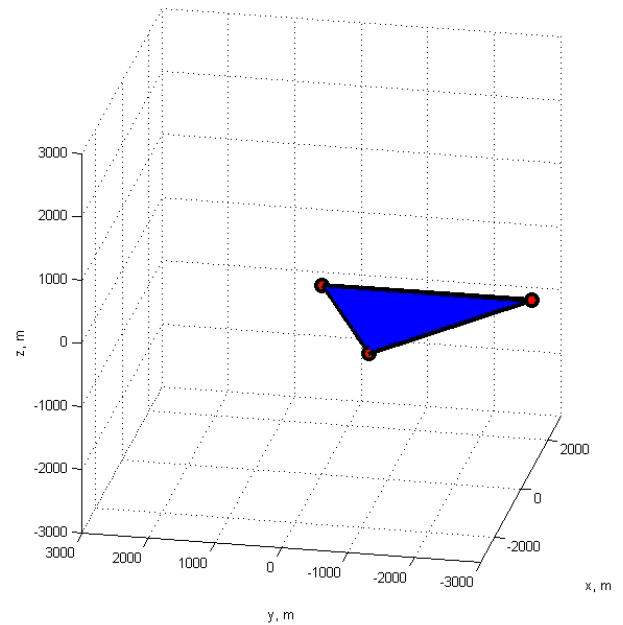
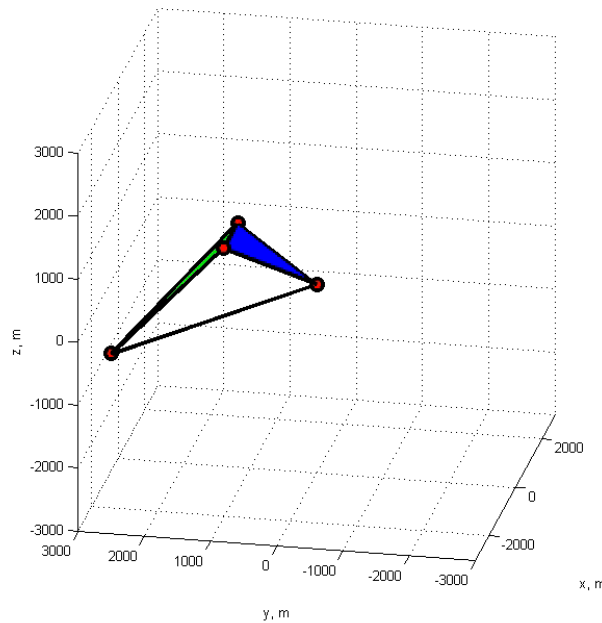
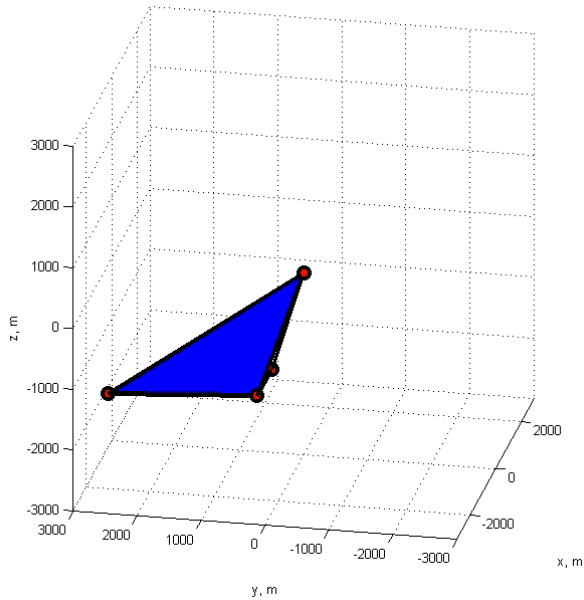
$$C_1(3A_1 - A_2 - A_3) + C_2(3A_2 - A_1 - A_3) + C_3(3A_3 - A_1 - A_2) = 0,$$

$$C_1(3B_1 - B_2 - B_3) + C_2(3B_2 - B_1 - B_3) + C_3(3B_3 - B_1 - B_2) = 0.$$

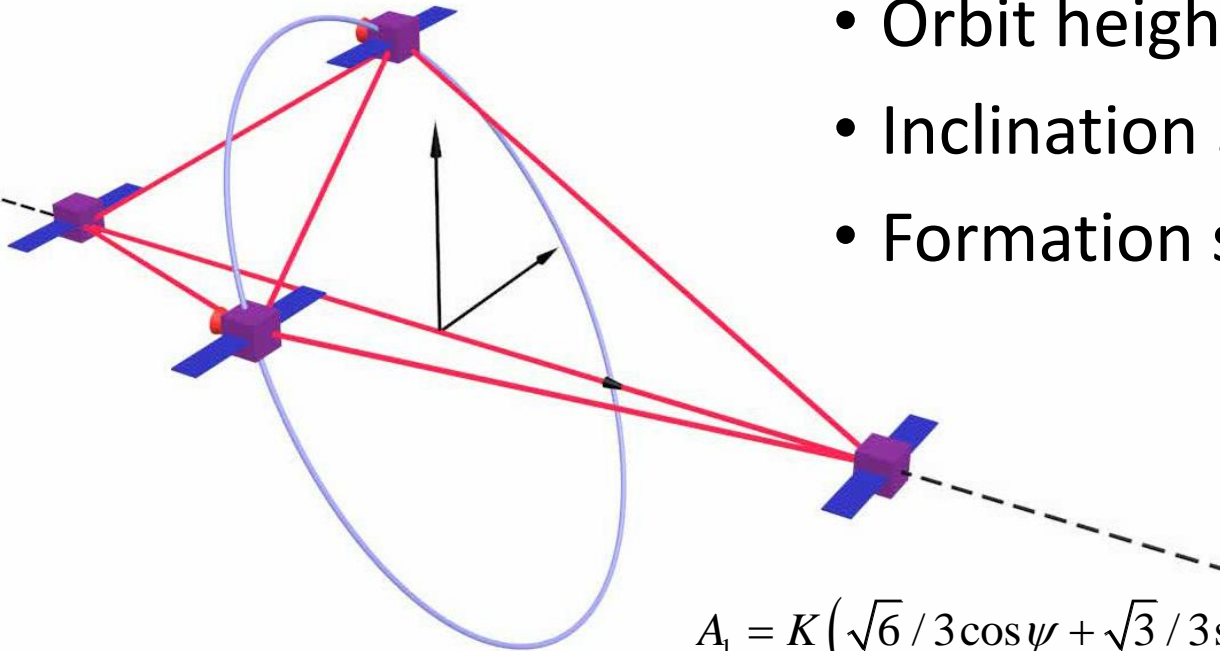
Quality/Volume conservation

Solutions are 7-parametric families

Some of the solutions are presented below



Focus on leader-follower formation



- Orbit height – 400 km
- Inclination 51.6 deg
- Formation size $K = 1000$ m

$$A_1 = K \left(\sqrt{6} / 3 \cos \psi + \sqrt{3} / 3 \sin \psi \right),$$

$$A_2 = K \left(\sqrt{6} / 3 \cos \psi - \sqrt{3} / 3 \sin \psi \right),$$

$$A_3 = 0,$$

$$B_1 = K \left(-\sqrt{3} / 3 \cos \psi + \sqrt{6} / 3 \sin \psi \right),$$

$$B_2 = K \left(\sqrt{3} / 3 \cos \psi + \sqrt{6} / 3 \sin \psi \right),$$

$$B_3 = 0.$$

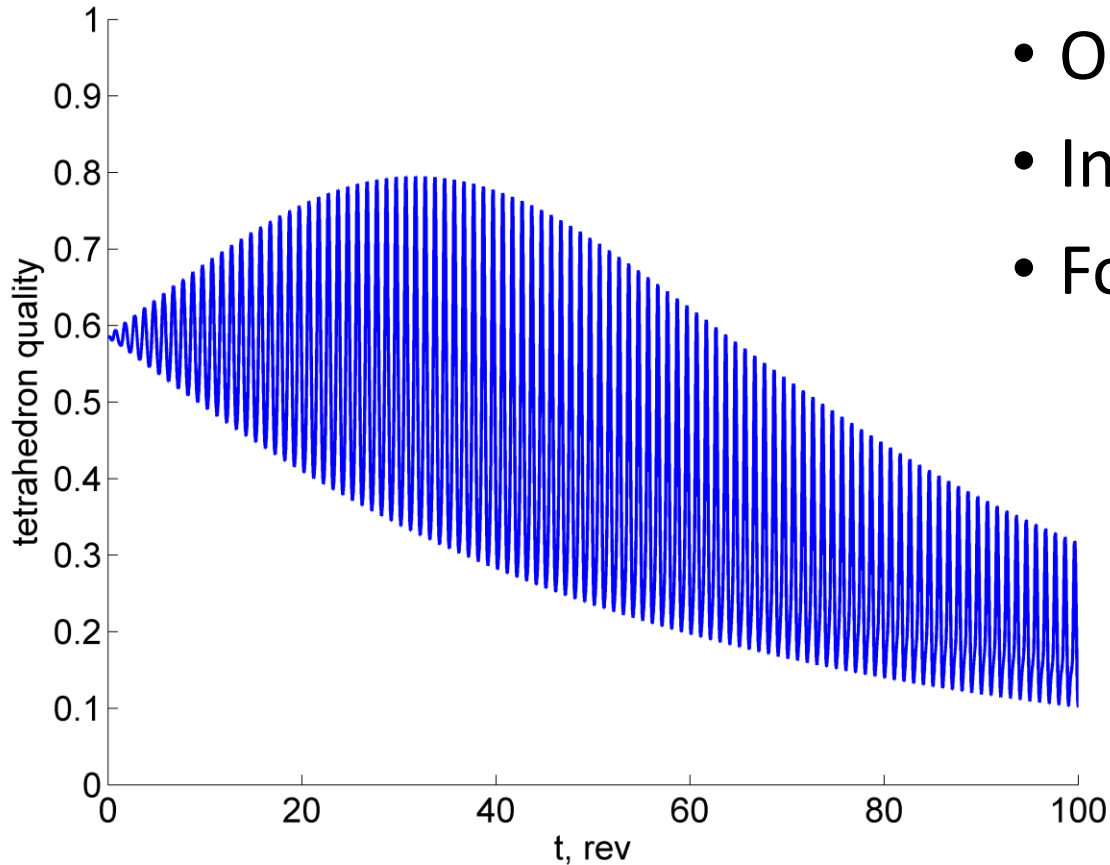
$$C_1 = C_2 = K \sqrt{\frac{5}{3}},$$

$$C_3 = 2K \sqrt{\frac{5}{3}}$$

$$\mathbf{D} = \sqrt{5}\mathbf{B},$$

$$\mathbf{E} = -\sqrt{5}\mathbf{A}$$

Focus on leader-follower formation



- Orbit height – 400 km
- Inclination 51.6 deg
- Formation size – 1000 m

Need to control formation

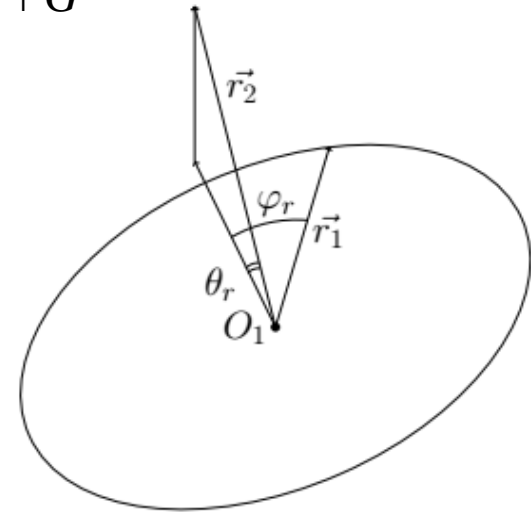
Using curvilinear coordinates

More natural to use and to describe relative motion

$$\begin{aligned} \frac{d^2}{dt^2} \rho - 2n \frac{d}{dt} (a_0 \varphi) - 3n^2 \rho &= 0 & \rho &= A \cos(nt + \gamma) + 2C, \\ \frac{d^2}{dt^2} (a_0 \varphi) + 2n \frac{d}{dt} \rho &= 0 & a_0 \varphi &= -2A \sin(nt + \gamma) - 3Cnt + G \\ \frac{d^2}{dt^2} (a_0 \theta) + n^2 (a_0 \theta) &= 0 & a_0 \theta &= B \sin(nt + \delta) \end{aligned}$$

We use the same set of initial conditions for leader-follower formation

Need to maintain amplitudes A,B and phase differences $\gamma_1 - \gamma_2 = \delta_1 - \delta_2 = \arccos(1/3)$



Osculating coordinates

New variables:

$$\rho = A \sin \psi + 2C,$$

$$\frac{d}{dt} \rho = An \cos \psi,$$

$$a_0 \theta = 2A \cos \psi + D,$$

$$\frac{d}{dt} (a_0 \theta) = -2An \sin \psi - 3C\omega,$$

$$a_0 \varphi = B \sin \lambda,$$

$$\frac{d}{dt} (a_0 \varphi) = Bn \cos \lambda.$$

The system is described by

$$\dot{A} = \frac{1}{n} \left((u_x + g_x) \cos \psi - 2(u_y + g_y) \sin \psi \right),$$

$$\dot{B} = \frac{1}{n} (u_z + g_z) \cos \lambda,$$

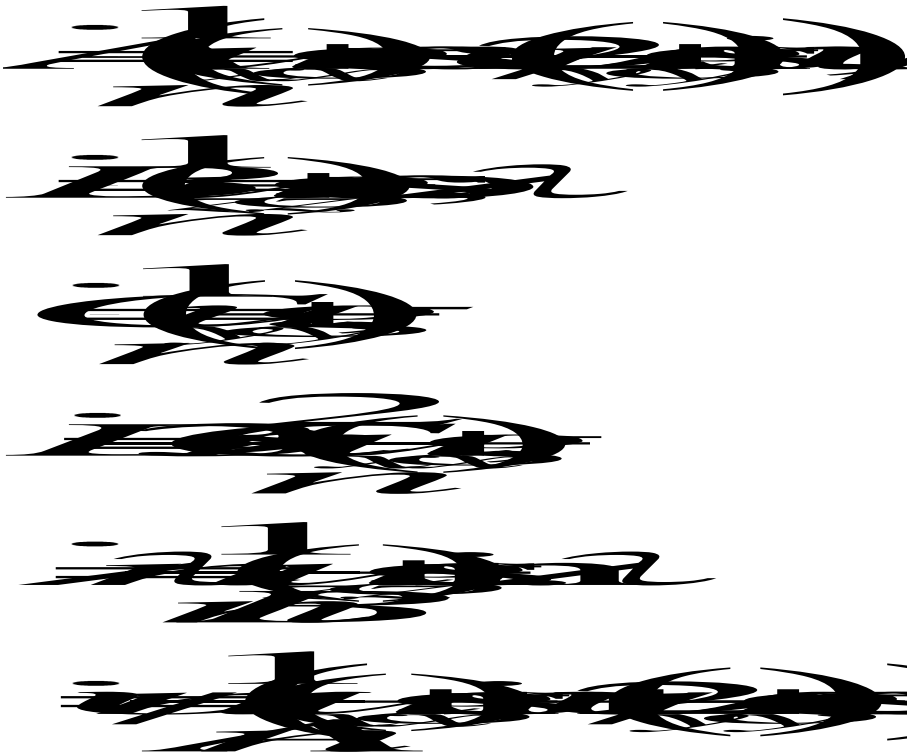
$$\dot{C} = \frac{1}{n} (u_y + g_y),$$

$$\dot{D} = -3Cn - \frac{2}{n} (u_x + g_x),$$

$$\dot{\lambda} = n - \frac{1}{nB} (u_z + g_z) \sin \lambda.$$

$$\dot{\psi} = n - \frac{1}{An} \left((u_x + g_x) \sin \psi + 2(u_y + g_y) \cos \psi \right).$$

Atmospheric control algorithm



- Asymptotically stable controller
- We neglect additional accelerations
- But acceleration is **only along velocity vector**

$$\dot{A} = \frac{-2u_y \sin \psi}{n},$$

$$\dot{C} = \frac{u_y}{n},$$

$$\dot{D} = -3Cn.$$

Atmospheric control algorithm

First step – shift adjust and drift elimination

$$C_{ref} = 0, \quad D_{ref} = D_0$$

- Direct Lyapunov method
- Control

$$V = C^2 + k_D (D - D_{ref})^2, \quad k_D > 0.$$

$$u_y = 3n^2 k_D (D - D_{ref}) - k_c C$$

Second step – phasing

- Control only if it helps to phase properly

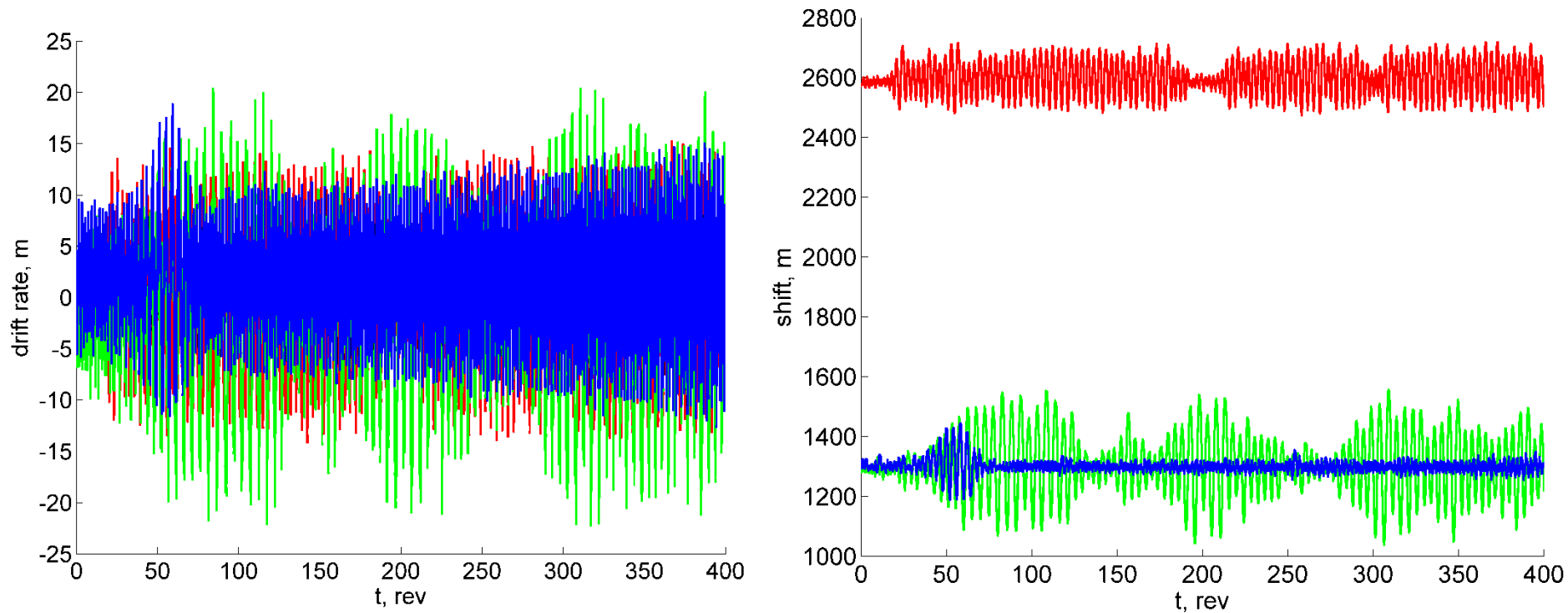
$$\text{if } \psi_2 - \psi_1 > \arccos(1/3),$$

$$\text{then control only if } u_y \cos \psi_1 < 0.$$

Third step – amplitudes A, B

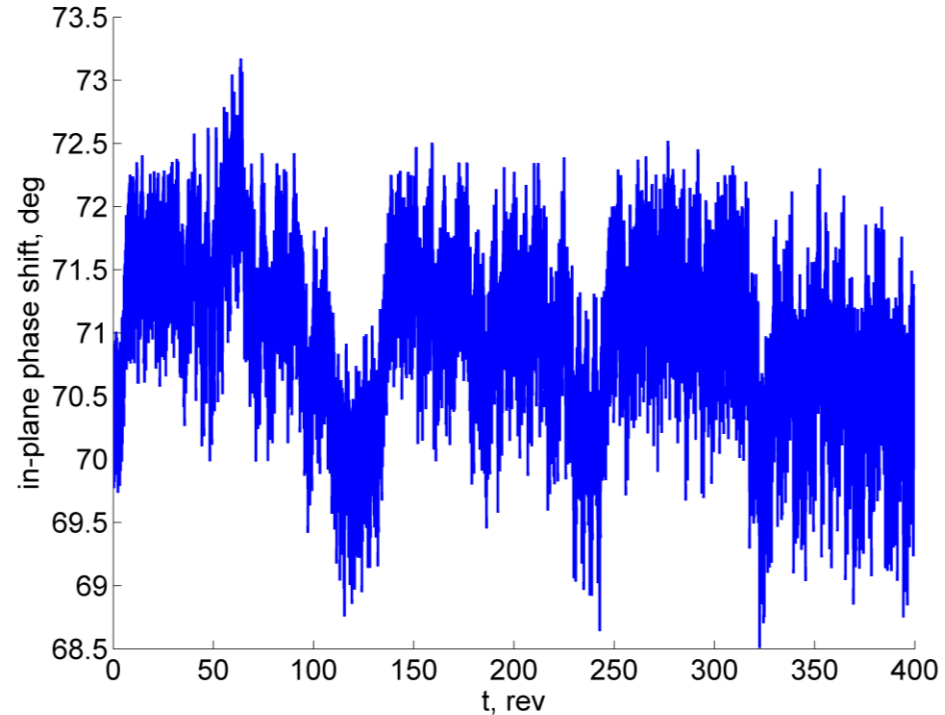
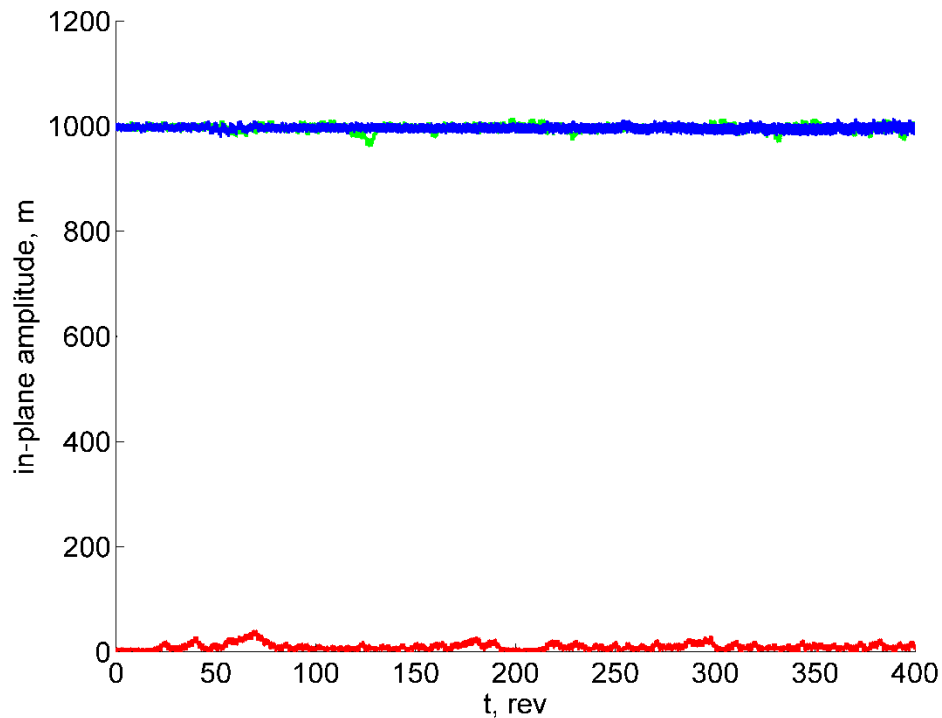
- The same, but if phasing is correct

Atmospheric control algorithm



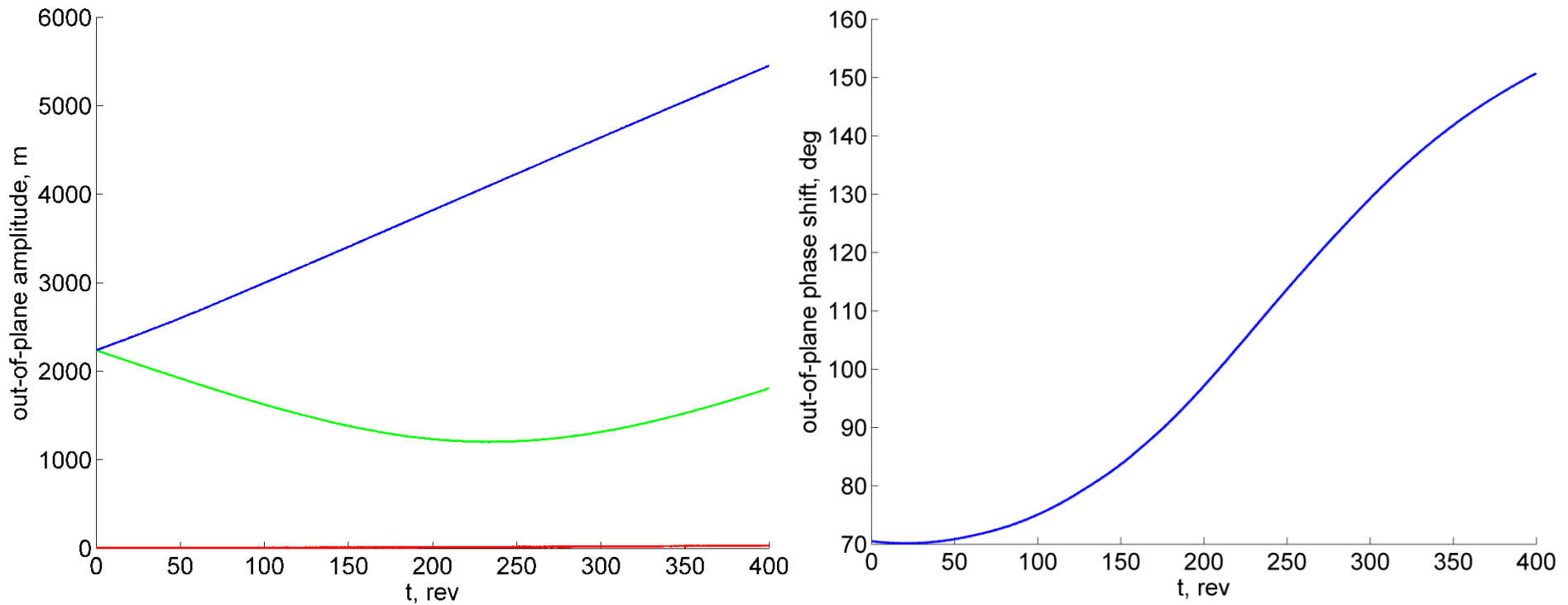
Drift and shift are controllable

Atmospheric control algorithm



In-plane motion is fully controllable

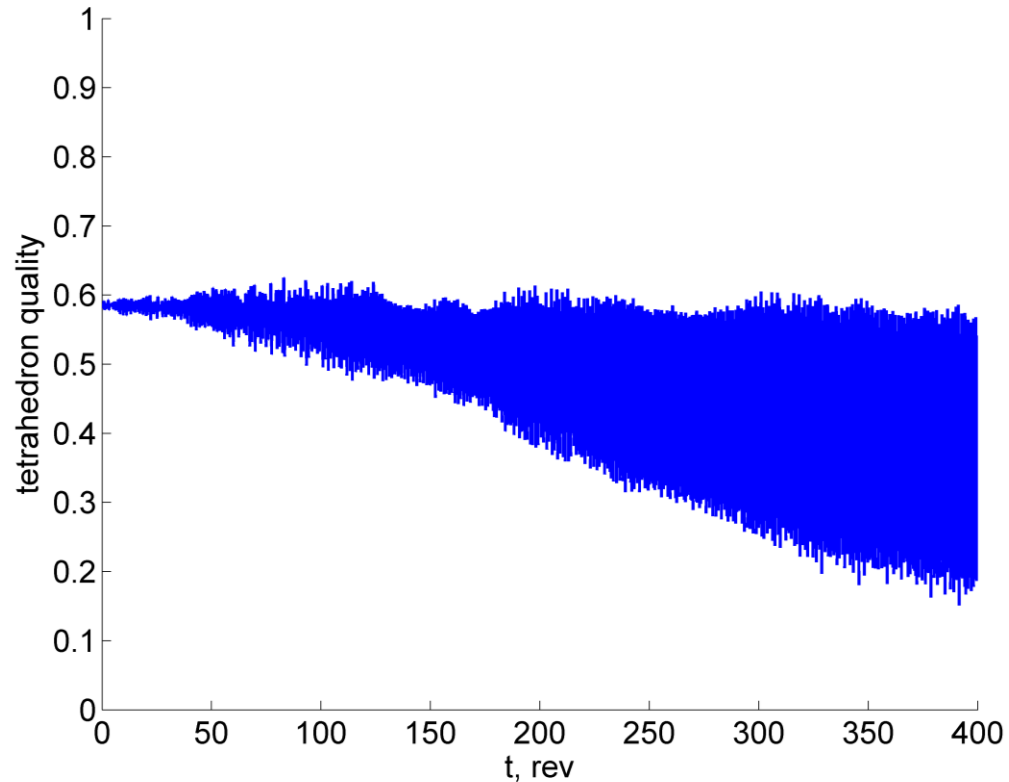
Atmospheric control algorithm



Out-of-plane motion is not controllable

Atmospheric control algorithm

- Tetrahedron configuration conserving quality in linear model
- Tetrahedron size $K = 1000$ m
- Orbit height = 400 km
- Masses = 5 kg
- Area = 0.15 m²
- Inclination = 51.6 deg
- Disturbances – J2 and atmosphere



Conclusions

- The reference orbit for 4 satellites conserving volume and shape of the tetrahedron is found in linear model on circular orbit
- Suggested Lyapunov-based controller can effectively control relative in-plane motion of the satellites, thus slowing degradation rate of the tetrahedron
- The out-of-plane motion is almost uncontrollable, because the lift force is too small
- It is possible to decelerate the degradation rate of relative parameters for several weeks

Questions?