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# Femtosatellites Swarm Motion Estimation Using Measurements of Communication Signal Magnitude

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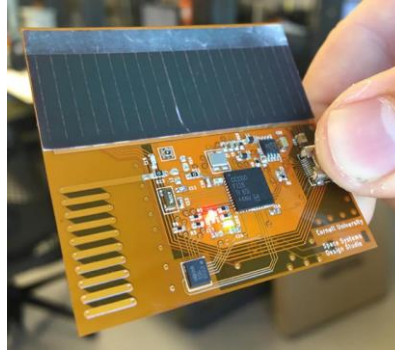
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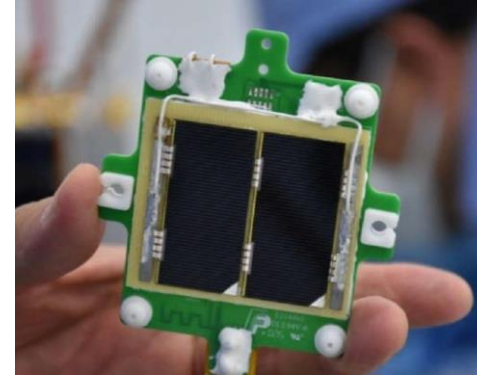
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# Introduction

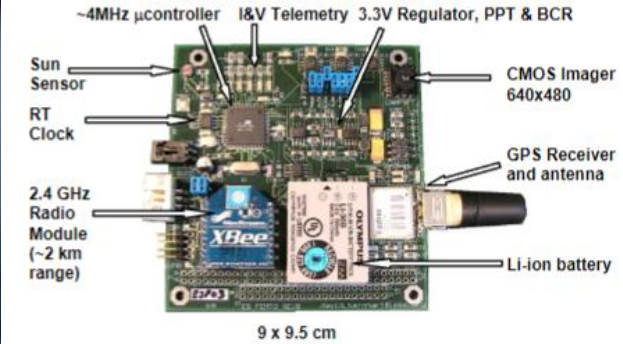
- Femtosatellite advantages
  - Multiple spatial measurements in orbit
  - Numerous of laboratory prototypes
  - Cheap production and launch
  - Lot of femtosats can be launched together



Hunter V.A., Peck M. R-Selected Spacecraft // Journal of Spacecraft and Rockets, V. 57, N. 1, 2020, pp. 90-98



Yang L. et. al. The design and experiment of stardust femto-satellite // Acta Astronautica, V. 174, 2020, pp. 72-81

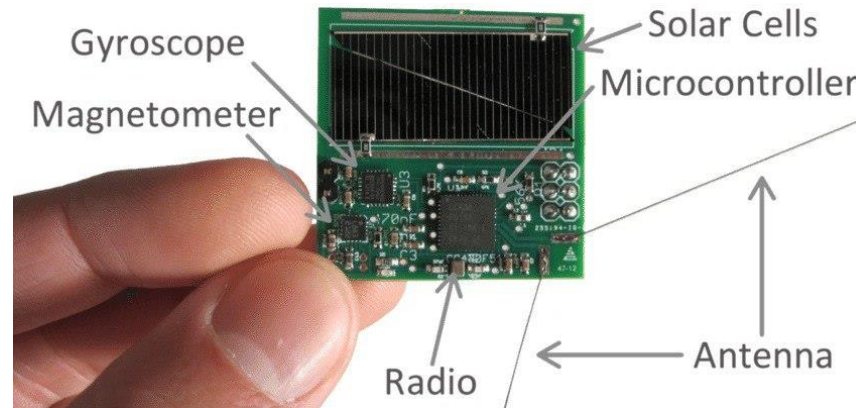


Barnhart D.J. et. al. A Low-cost Femtosatellite Enable Distributed Space Missions // Proceedings of 57th International Astronautical Congress, 2012, pp. 1-15

- Motivation for novel algorithm for relative navigation
  - Low power supply
  - GNSS-based navigation is inappropriate
  - Angles only camera-based navigation is characterized by unobservability



Communication antenna-based navigation should be investigated



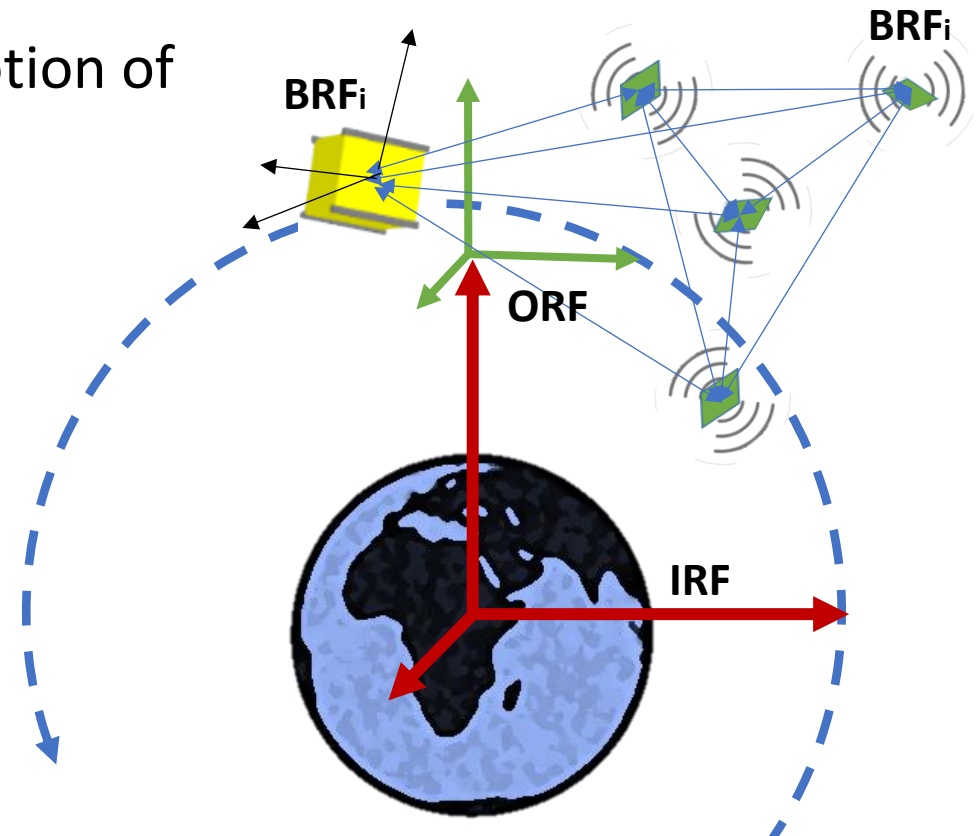
Manchester Z. Peck M., Filo A. KickSat: A Crowd-Funded Mission To Demonstrate The World's Smallest Spacecraft // 27th Annual AIAA/USU Conference on Small Satellites, 2013, pp. 1-9



Hu, Z., Timmons, T., Stamat, L. and McInnes, C. Development of a 10g Femto- satellite with Active Attitude Control // 17th Reinventing Space Conference, Belfast, Northern Ireland, 12-14 Nov 2019, pp. 1-7.

# Problem statement

- Considered:
  - Chief satellites with known orbital and attitude motion at near circular orbit
  - Deputy femtosatellites deployed from chief satellites
  - Antennas of the satellites in the swarm are isotropic or half-wave antennas
  - Deputy femtosatellites attitude is considered known
- It is necessary to estimate relative translational motion of femtosatellites swarm relative to chief satellites
- Reference frames:
  - Inertial (IRF)
  - Orbital (ORF)
  - Body (BRF)



# Motion system and measurement system

- Motion equations:

$$\begin{cases}
 \dot{\mathbf{r}} = \mathbf{v}, & \text{Orbital motion in ORF} \\
 \dot{v}_x = -2\omega_0 v_z - \frac{\rho C_d}{2m} S (v_{orb} + v_x)^2 (\lambda_x \lambda_y - \lambda_0 \lambda_z), \\
 \dot{v}_y = -\omega_0^2 y, & \text{Aerodynamic drag} \\
 \dot{v}_z = 3\omega_0^2 z + 2\omega_0 v_x, \\
 \dot{\boldsymbol{\lambda}} = \frac{1}{2} \boldsymbol{\lambda} \circ \boldsymbol{\omega}, & \text{Attitude motion in IRF} \\
 \mathbf{I} \dot{\boldsymbol{\omega}} + \boldsymbol{\omega} \times \mathbf{I} \boldsymbol{\omega} = \mathbf{M}_{ext}.
 \end{cases}$$

$\boldsymbol{\lambda} = [\lambda_0, \lambda_x, \lambda_y, \lambda_z]$ : Attitude quaternion

$\omega_0$ : Angular velocity of ORF center in IRF

$v_{orb}$ : Translational velocity of ORF center in IRF

$\mathbf{I}$ : Satellite inertia tensor

$\mathbf{M}_{ext}$ : External torque

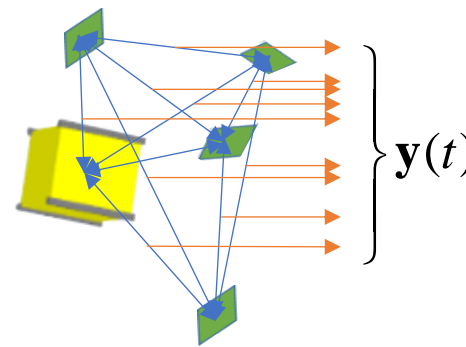
- State vector of N femtosatellites to find:

$$\mathbf{x} = [\mathbf{r}_1^T, \mathbf{v}_1^T, \dots, \mathbf{r}_N^T, \mathbf{v}_N^T]^T$$

- Measurements vector of  $M+N(N-1)/2$  RSSI (received signal strength indicator) between  $M$  chief and  $N$  deputy:

$$\mathbf{y} = [y_{c_1-d_1}, \dots, y_{c_M-d_N}, y_{d_1-d_2}, \dots, y_{d_{N-1}-d_N}]$$

- Model of antenna signal



$$P_R = P_T G_R G_T \frac{\lambda^2}{4\pi r^2}, \quad \tilde{r}^2 = \frac{4\pi P_R}{\lambda^2 P_T} = \frac{r^2}{G_R G_T},$$

Measurement model:

$$y = \tilde{r} + \delta r = \frac{r}{\sqrt{G_R G_T}} + \delta r,$$

$G \equiv 1$ , Isotropic antenna

$$G = \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta}, \quad \text{Half-wave antenna}$$



# Analytical observability of the system

- Sufficient observability criteria: the system  $\begin{cases} \dot{\mathbf{x}} = \mathbf{f}(t, \mathbf{x}), \\ \mathbf{y} = \mathbf{h}(t, \mathbf{x}) \end{cases}$  is observable on  $[t_0, t_1]$ , if:

1.  $km = n$ , where  $n$ : Length of state vector  
 $m$ : Length of measurement vector  
 $k$ : Number of existing derivatives

2. Mapping of observability  $\mathbf{H}$  is differentiable:

$$\mathbf{H} = \begin{bmatrix} \mathbf{y} \\ \vdots \\ \frac{d^{k-1}\mathbf{y}}{(dt)^{k-1}} \end{bmatrix} \quad \mathbf{J} = \frac{\partial \mathbf{H}}{\partial \mathbf{x}_0} = \begin{bmatrix} \frac{\partial y}{\partial x_0^1} & \cdots & \frac{\partial y}{\partial x_0^n} \\ \vdots & \ddots & \vdots \\ \frac{\partial y^{(k-1)}}{\partial x_0^1} & \cdots & \frac{\partial y^{(k-1)}}{\partial x_0^n} \end{bmatrix}$$

The system is locally observable over the interval  $[0, T]$  if the mapping from the initial state  $x_0$  to output profile  $y(t)$  ( $t \in [0, T]$ ) is local bijection (i.e., if the initial state can be reconstructed by the outputs on this interval)

Bartosiewicz, Z., "Local Observability of Nonlinear Systems," Systems & Control Letters, Vol. 25, No. 4, 1995, pp. 295–298. doi:10.1016/0167-6911(94)00074-6

3. The Jacobi matrix  $\mathbf{J}$  satisfies the uniform ratio of the major minors:

$$\exists \varepsilon > 0 \rightarrow |\Delta_1| \geq \varepsilon, \quad \frac{|\Delta_2|}{|\Delta_1|} \geq \varepsilon, \quad \dots \quad \frac{|\Delta_n|}{|\Delta_{n-1}|} \geq \varepsilon \quad \forall x \in E^n$$



## Numerical observability of the system

- Criteria of observability: the system 
$$\begin{cases} \dot{\mathbf{x}} = \mathbf{f}(t, \mathbf{x}) \\ \mathbf{y} = \mathbf{h}(t, \mathbf{x}) \end{cases}$$

Andrew J. Whalen "Observability and Controllability of Nonlinear Networks: The Role of Symmetry"

is observable if and only if  $\exists k \Rightarrow$  singular numbers are equal in modulus :

$$g(\mathbf{x}) = 1, \quad \text{where} \quad g(\mathbf{x}) = \frac{|\sigma_{\min}(\mathbf{J}^T \mathbf{J})|}{|\sigma_{\max}(\mathbf{J}^T \mathbf{J})|}$$

$\sigma$  – singular numbers

- If  $g(\mathbf{x}) < 1$  it cannot be stated that system does not local observable
- Some empirical criteria can be used. For example, can be introduced a threshold  $P$  to separate the observed subspace in state vector space:

$$\sigma_1, \dots, \sigma_j > P,$$

For observed subspace

$$\sigma_{j+1}, \dots, \sigma_n \leq P$$

For unobserved subspace

## Extended Kalman filter application

- Linearized dynamic model
- Linearized measurement model
- Prediction step

$$\mathbf{x}_k^- = \Phi_k \mathbf{x}_{k-1}$$

$$P_k^- = \Phi_k P_{k-1} \Phi_k^T + Q^-$$

$$Q^- = \int \Phi_k D Q D^T \Phi_k^T dt$$

- Update step

$$K = P_k^- H_k^T (H_k P_k^- H_k^T + R)$$

$$\mathbf{x}_k = \mathbf{x}_{k-1} + K (\mathbf{y}_k^{real} - \mathbf{y}_k^{model})$$

$$P_k = (E - KH_k) P_k^-$$

$$\begin{cases} \mathbf{x}_k^- = \Phi_k \mathbf{x}_{k-1}, \\ \mathbf{y}_k = H \mathbf{x}_k + \mathbf{v}_k. \end{cases}$$

$$\tilde{\mathbf{y}} = \frac{|\mathbf{r}_{deputy} - \mathbf{r}_{chief}|}{\sqrt{G_R G_T}}$$

$$\Phi = \begin{bmatrix} \Phi_1 & \dots & 0_{12 \times 12} \\ \dots & \ddots & \dots \\ 0_{12 \times 12} & \dots & \Phi_n \end{bmatrix}$$

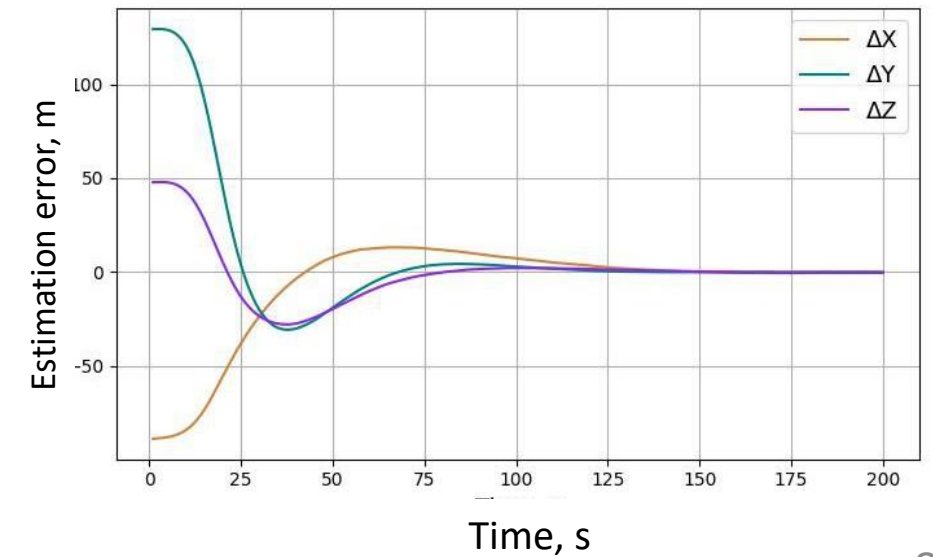
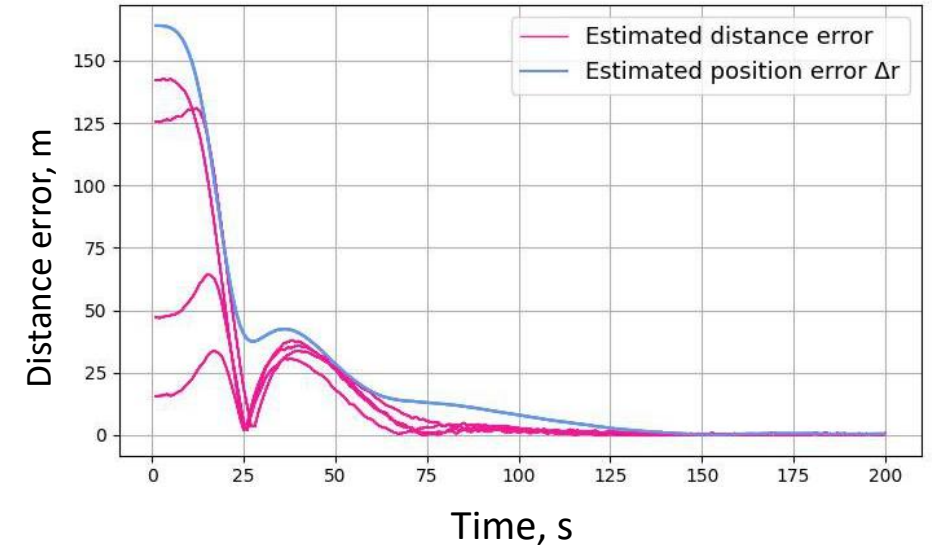
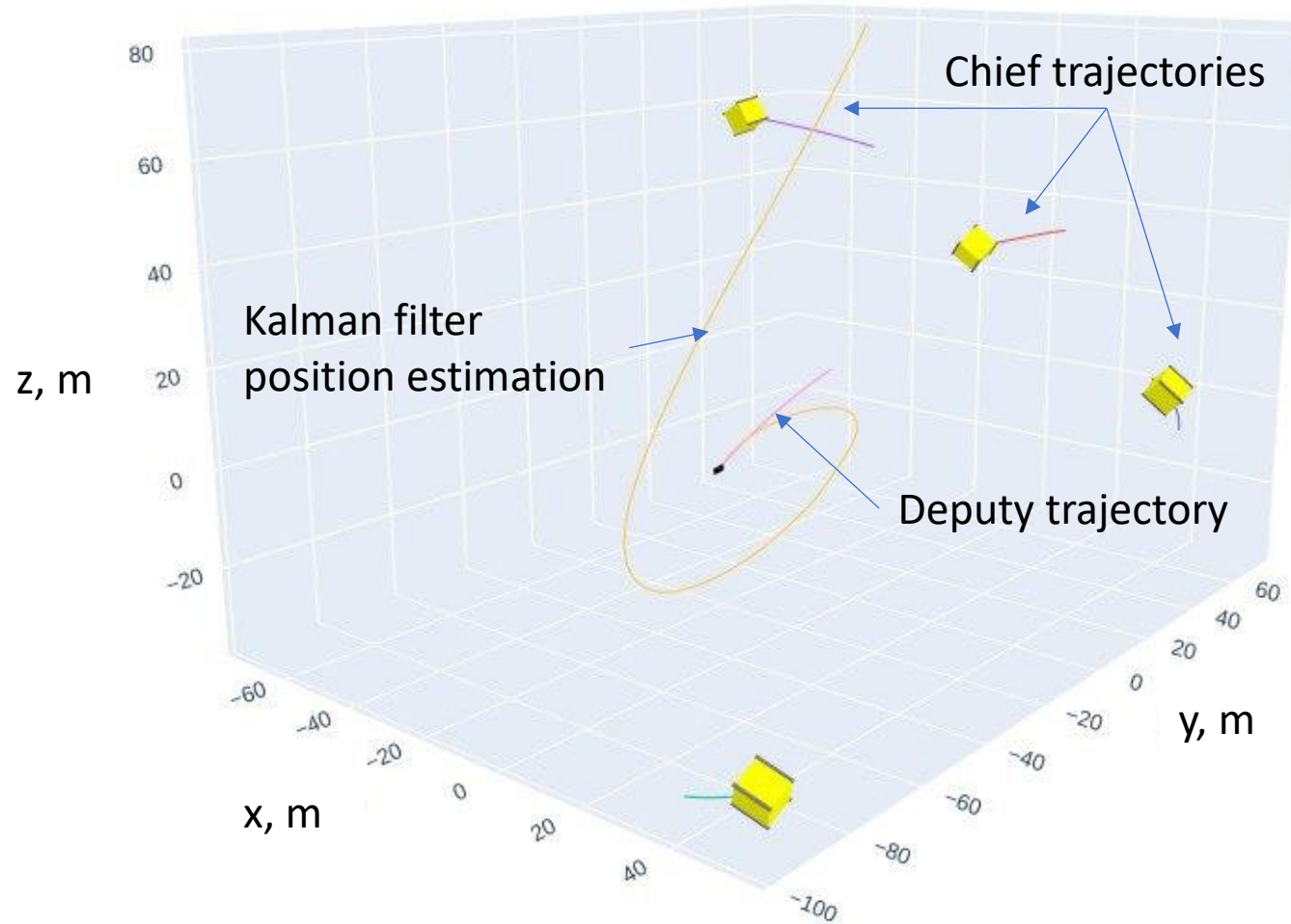
$$P(t=0) = \begin{bmatrix} P_1 & \dots & 0_{12 \times 12} \\ \dots & \ddots & \dots \\ 0_{12 \times 12} & \dots & P_1 \end{bmatrix}$$

$$Q = \begin{bmatrix} Q_1 & \dots & 0_{6 \times 6} \\ \dots & \ddots & \dots \\ 0_{6 \times 6} & \dots & Q_1 \end{bmatrix}$$



## Example of the system with full observability

- 4 chief spacecrafts and 1 deputy femtosatellite
- Isotropic antennas  $G \equiv 1$
- State vector  $\mathbf{x} = [\mathbf{r}_1^T, \mathbf{v}_1^T]^T$

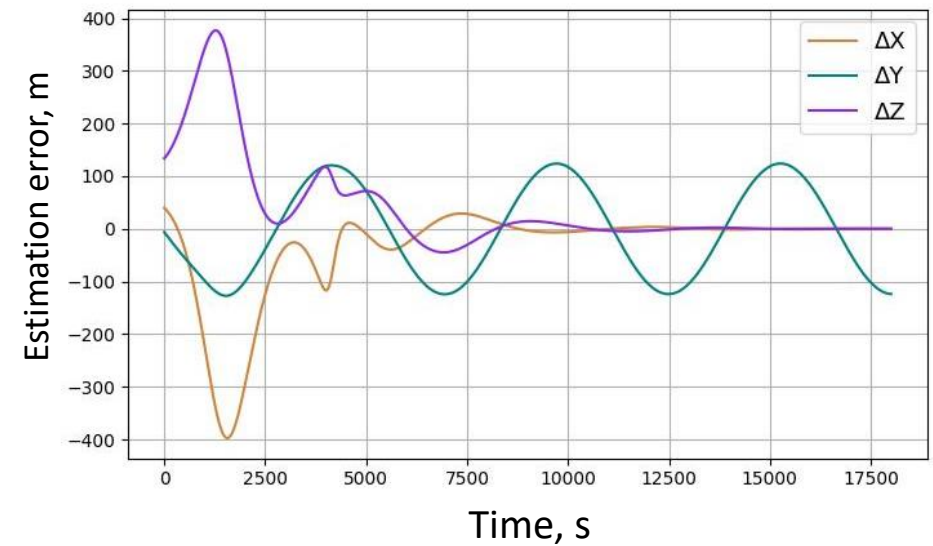
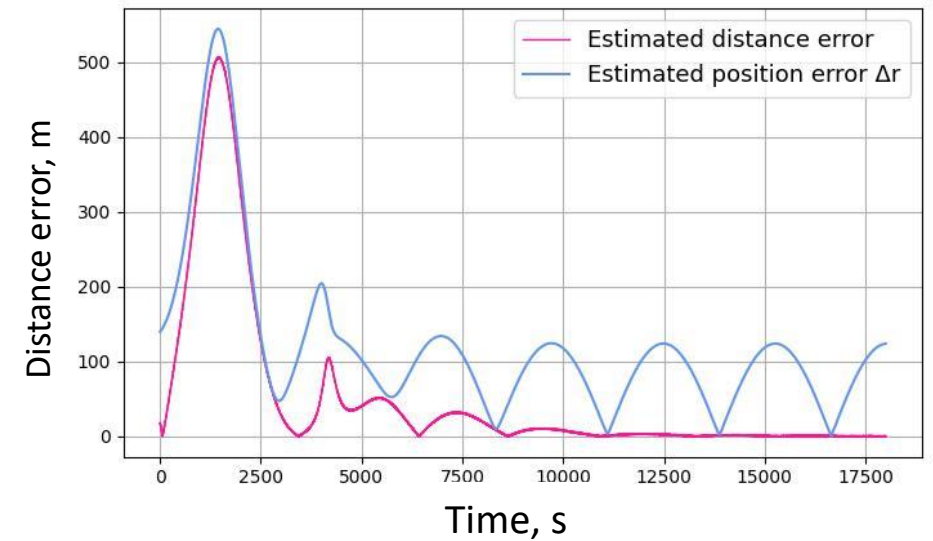
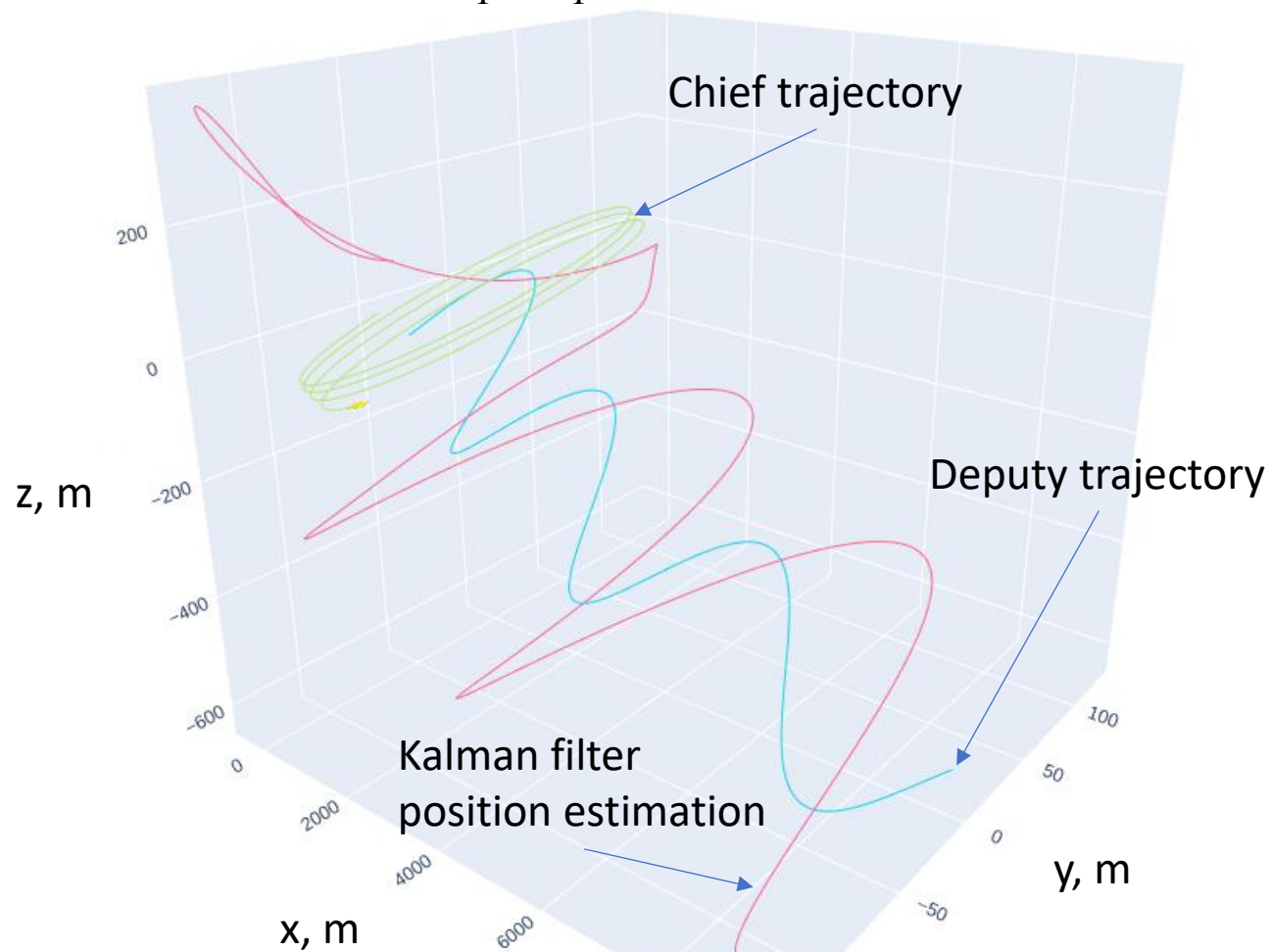






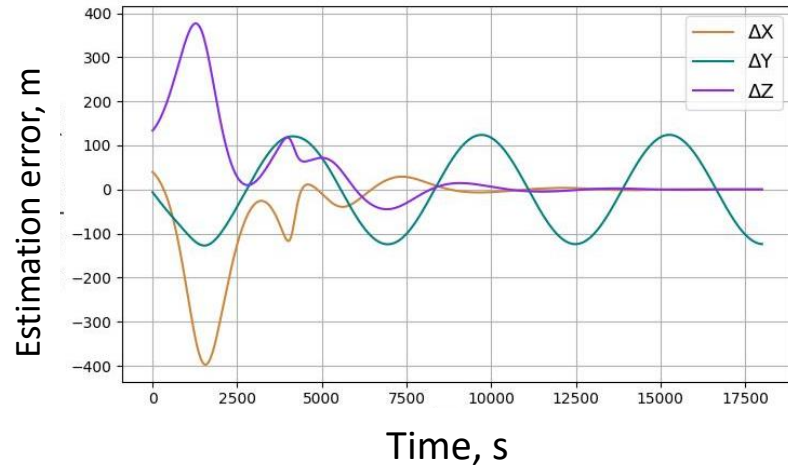
## Example of the system with local observability

- 1 chief and 1 deputy
- Isotropic antennas  $G \equiv 1$
- State vector  $\mathbf{x} = [\mathbf{r}_1^T, \mathbf{v}_1^T]^T$



# Local observability of the system

- 1 chief and 1 deputy



$$\mathbf{x} = [x, y, z, v_x, v_y, v_z] \rightarrow \mathbf{x} = [x, z, v_x, v_z]$$

Singular values:  $\sigma \approx [1, 1, 10^{-2}, 10^{-12}]$

The uniform ratio of the minors is not fulfilled (there is no sufficient observability condition)

Numerical modeling



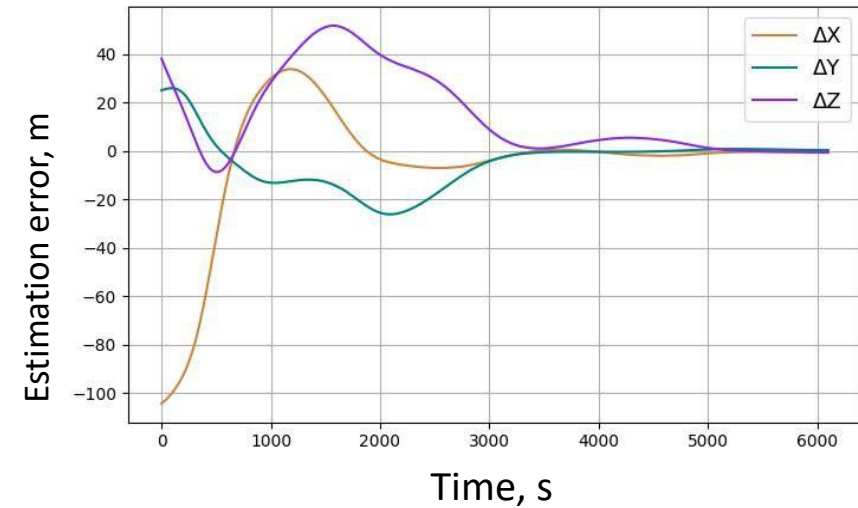
System is unobservable

The uniform ratio of the minors is fulfilled

$$\downarrow \frac{|\Delta_i|}{|\Delta_{i-1}|} \geq 10^{-6} \sim 10^{-5}$$

System is locally observable

- 2 chiefs and 1 deputy



State vector:  $\mathbf{x} = [x, y, z, v_x, v_y, v_z]$

Singular values:  $\sigma \approx [1, 1, 10^{-1}, 10^{-1}, 10^{-3}, 10^{-6}]$

The uniform ratio of the minors is fulfilled



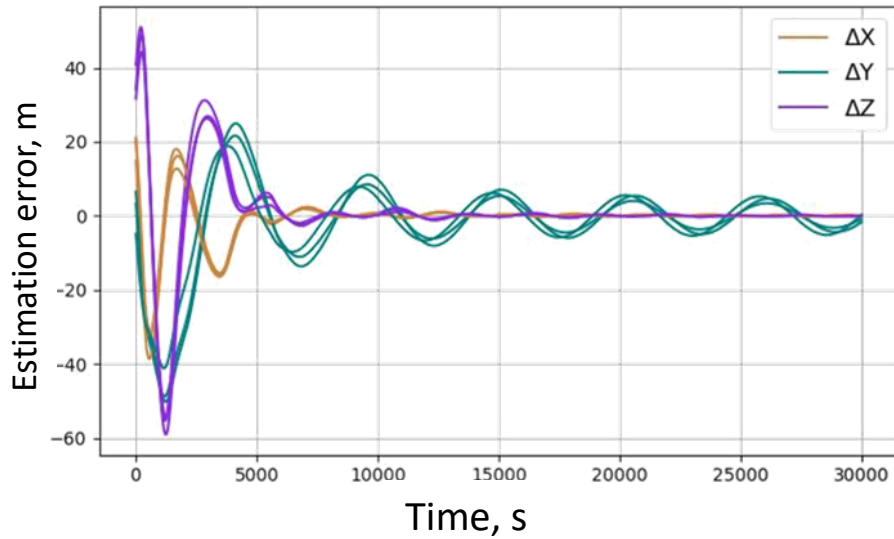
System is fully observable

$$\frac{|\Delta_i|}{|\Delta_{i-1}|} \geq 10^{-5} \sim 10^{-4}$$



# Local observability depending on chiefs relative motion

- 2 chiefs satellites and 3 deputies
- Relative distance between the chiefs is 50-100m



State vector:

$$\mathbf{x} = [x, y, z, v_x, v_y, v_z]$$

Singular values:

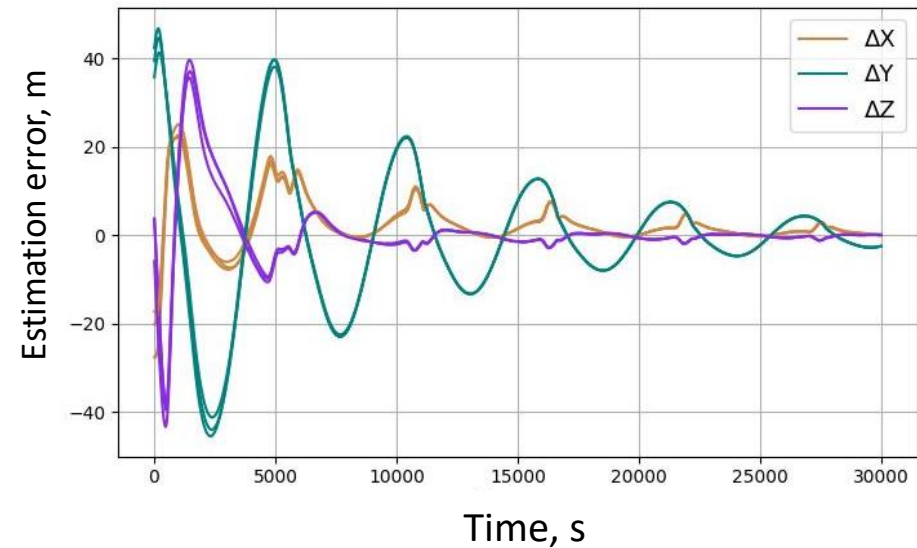
$$\sigma \approx [1, 1, 10^{-1}, 10^{-1}, 10^{-6}, 10^{-12}]$$

The uniform ratio of the minors is not fulfilled

$$\frac{|\Delta_4|}{|\Delta_5|} < 10^{-12}$$

System is locally observable

- Relative distance between the chiefs is 200-400m



State vector:

$$\mathbf{x} = [x, y, z, v_x, v_y, v_z]$$

Singular values:

$$\sigma \approx [1, 1, 10^{-1}, 10^{-1}, 10^{-3}, 10^{-6}]$$

The uniform ratio of the minors is fulfilled

System is fully observable

$$\frac{|\Delta_i|}{|\Delta_{i-1}|} \geq 10^{-5} \sim 10^{-4}$$

# Next steps: case of anisotropic antennas

- Relative motion observability including the deputies attitude motion using case of anisotropic antennas is currently under the investigation

- 1 chief spacecrafts and 1 deputy femtosatellite

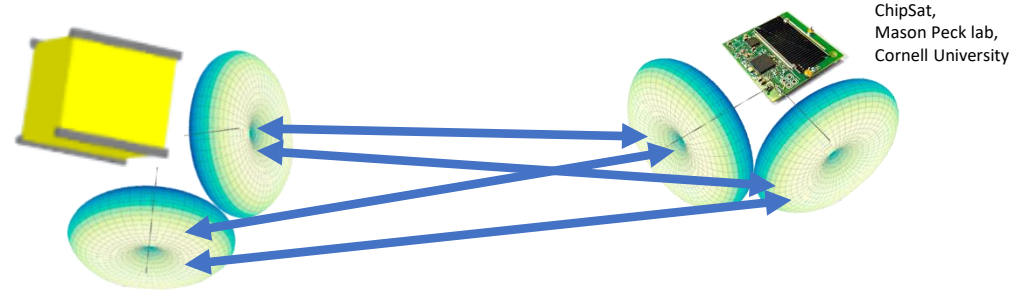
- Half-wave dipole antennas model  $G = \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta}$

- State vector  $\mathbf{x} = [\mathbf{r}_1^T, \mathbf{v}_1^T, \boldsymbol{\lambda}_1^T, \boldsymbol{\omega}_1^T]^T$

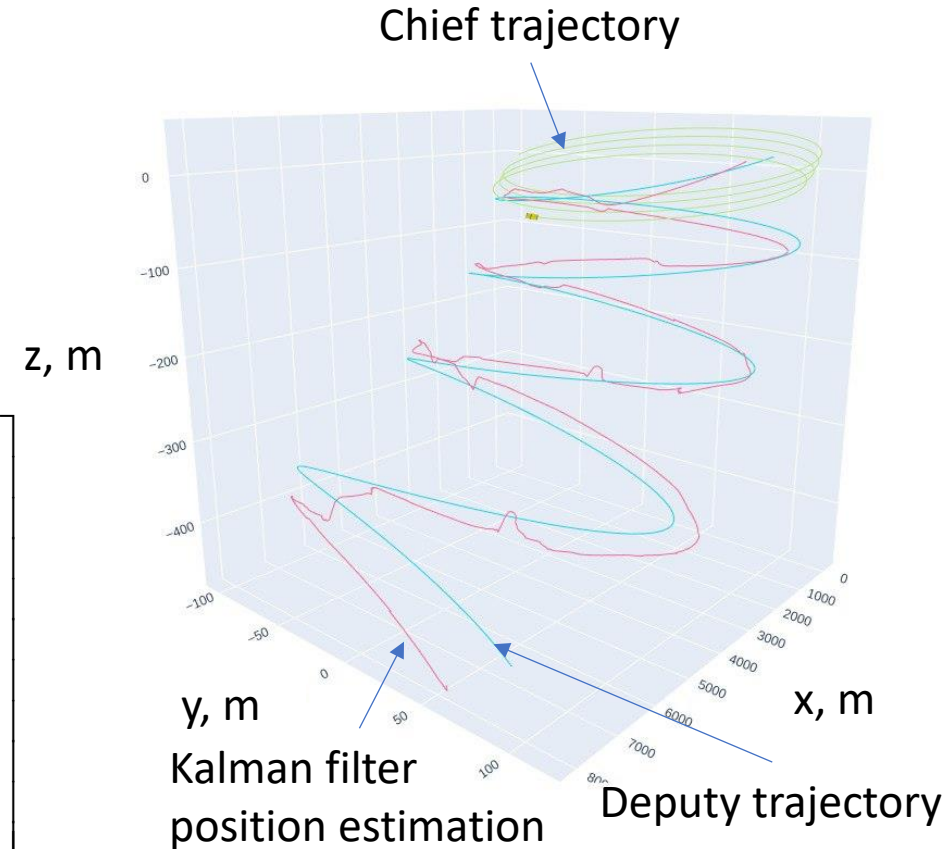
- System matrix and measurement matrix:

$$\Phi_1 = \begin{bmatrix} E_{3 \times 3} & 0_{3 \times 3} & E_{3 \times 3} \cdot dt & 0_{3 \times 3} \\ 0_{3 \times 3} & E_{3 \times 3} & 0_{3 \times 3} & E_{3 \times 3} \cdot \frac{dt}{2} \\ A & 0_{3 \times 3} & B & 0_{3 \times 3} \\ 0_{3 \times 3} & 0_{3 \times 3} & 0_{3 \times 3} & C \end{bmatrix}$$

$$H = \frac{\partial \mathbf{z}}{\partial \mathbf{x}} = \begin{bmatrix} H_{1,1}^{cd} & H_{1,2}^{cd} & \dots & \dots & H_{1,N}^{cd} \\ \dots & \dots & \dots & \dots & \dots \\ H_{M,1}^{cd} & H_{M,2}^{cd} & \dots & \dots & H_{M,N}^{cd} \\ H_{1,2}^{dd} & H_{2,1}^{dd} & 0_{N \times L_z} & \dots & 0_{N \times L_z} \\ H_{1,3}^{dd} & 0_{N \times L_z} & H_{3,1}^{dd} & \dots & 0_{N \times L_z} \\ \dots & \dots & \dots & \dots & \dots \\ 0_{N \times L_z} & 0_{N \times L_z} & 0_{N \times L_z} & \dots & H_{N-1,N}^{dd} \end{bmatrix}$$



ChipSat,  
Mason Peck lab,  
Cornell University





## Conclusions

- Possibility of relative motion estimation using measurements of communication signal magnitude is studied in this paper
- It is shown that for the case of isotropic antennas the system with one chief satellite is locally observable, and in case of two chiefs satellites the system is fully observable
- Depending on relative distance of two chiefs the uniform ratio of the minors can be not fulfilled and the system can be not observable
- As continuation of this study the case of measurements of anisotropic antennas signal magnitude is under the investigation

This study is supported by Russian Science Foundation, grant #24-11-00038,  
<https://rscf.ru/project/24-11-00038/>



**Thank you for your attention!**