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Asymptotic Relative Dynamics for Spacecraft on Close Hyperbolic Trajectories

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MOTIVATION: HYPERBOLIC TRAJECTORIES IN REAL MISSIONS

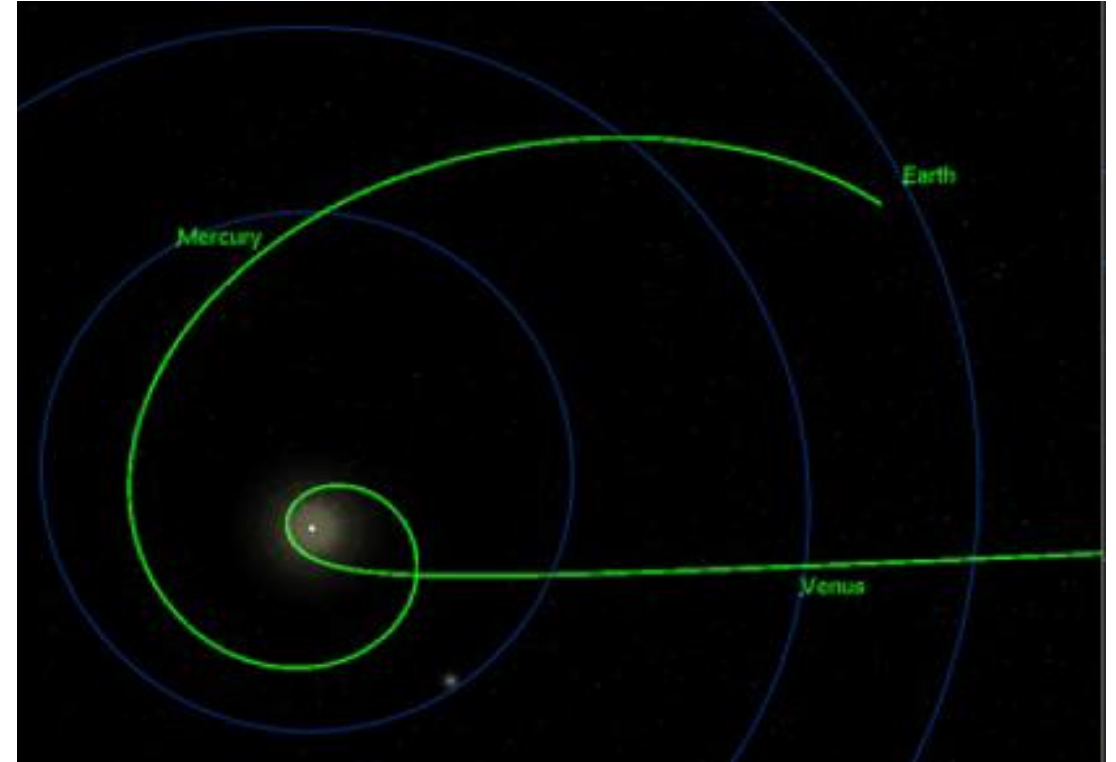
Past missions

- Pioneer 10 & 11
- Voyager 1 & 2
- New Horizons

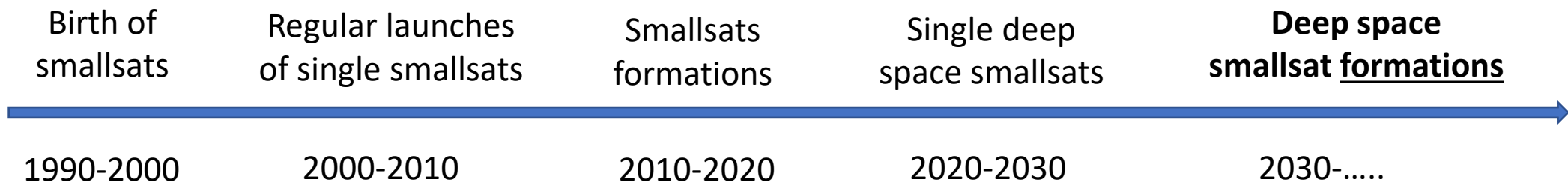
Future mission concepts

- Interstellar Probe mission
- Solar Gravitational Lens' Focus mission
- “Sundiver” concept

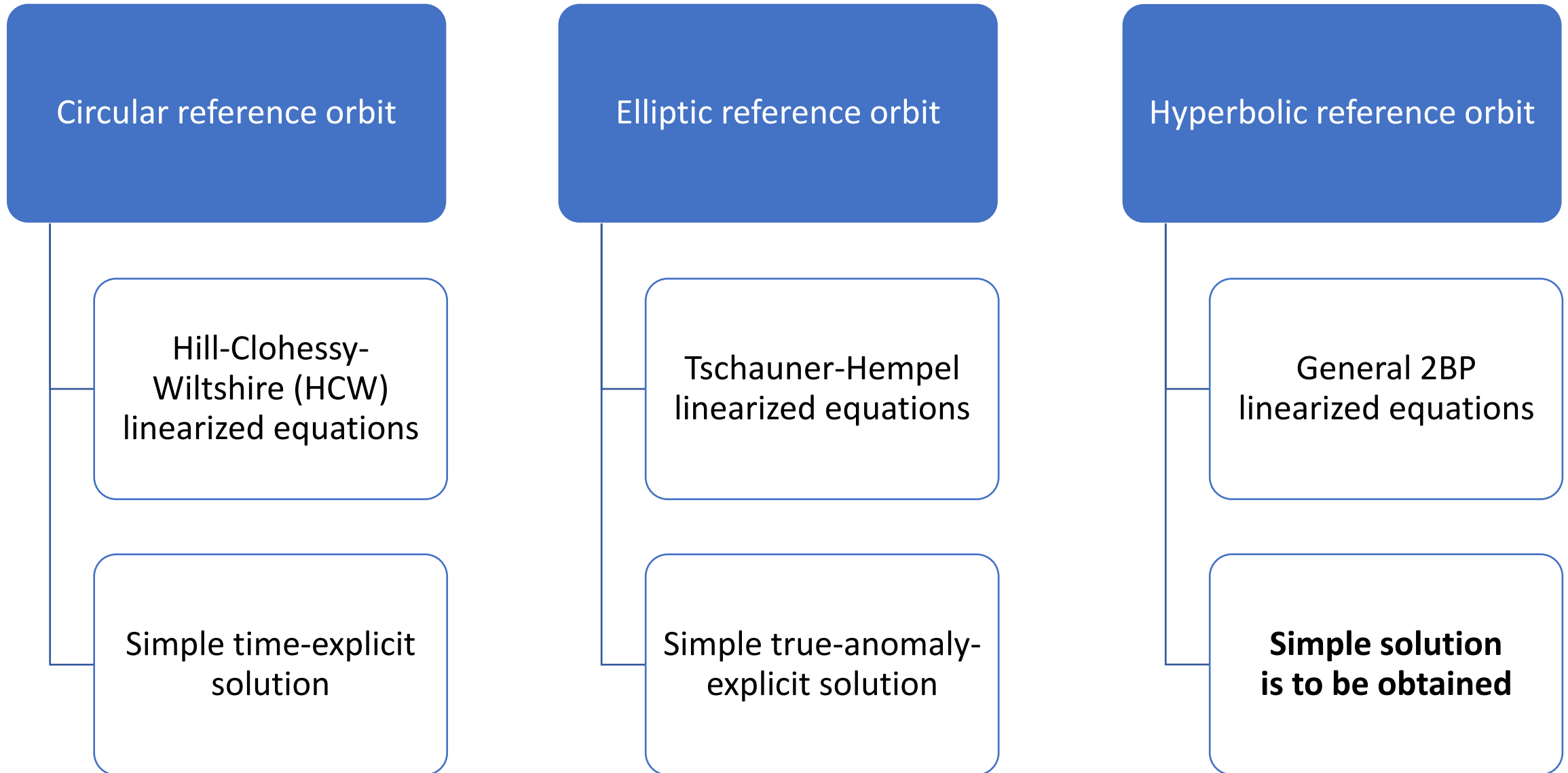
Smallsats and their formations have great potential for deep space exploration



Possible trajectory of the SGLF mission implementing the “Sundiver” concept



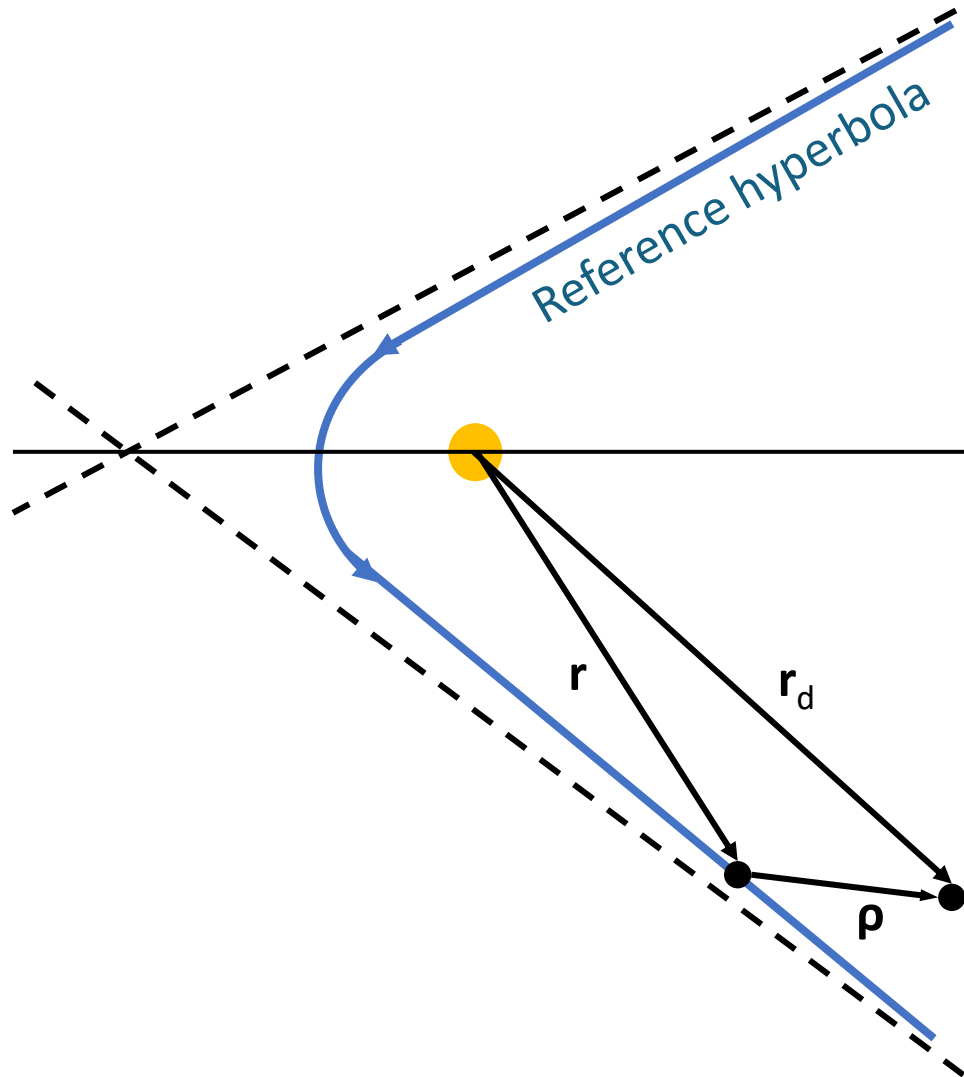
CIRCULAR vs ELLIPTIC vs HYPERBOLIC RELATIVE MOTION



GOALS OF STUDY

1. To obtain a *practical description* of a relative motion in close hyperbolas
2. To find out *what types* of a hyperbolic relative motion are possible
3. To demonstrate *how to design* a formation in close hyperbolic trajectories

EQUATIONS OF KEPLERIAN RELATIVE MOTION



\mathbf{r} – chief's radius-vector

\mathbf{r}_d – deputy's radius-vector

$\boldsymbol{\rho} = \mathbf{r}_d - \mathbf{r}$ – the relative position vector

Each spacecraft moves along a hyperbola with the Sun at the focus; spacecraft do not interact

$$\ddot{\mathbf{r}} = -\frac{\mu\mathbf{r}}{r^3} \quad \ddot{\mathbf{r}}_d = -\frac{\mu\mathbf{r}_d}{r_d^3} \quad \ddot{\boldsymbol{\rho}} = \ddot{\mathbf{r}}_d - \ddot{\mathbf{r}}$$

Linearization under the assumption $\frac{\rho}{r} \ll 1$

$$\ddot{\boldsymbol{\rho}} = -\frac{\mu}{r^3} \left(\boldsymbol{\rho} - \frac{3(\mathbf{r} \cdot \boldsymbol{\rho})\mathbf{r}}{r^2} \right)$$

ASYMPTOTIC COORDINATE SYSTEM AND δ VARIABLE

Assume we know the reference hyperbola $(a, e, i, \Omega, \omega, \tau)$

We define the Asymptotic Coordinate System (ACS) as following

- The origin – the attractive center (the Sun)
- \mathbf{e}_1 – along the outgoing asymptote
- \mathbf{e}_2 – complement to the right-handed basis
- \mathbf{e}_3 – along the orbital angular momentum

We introduce a new angle δ

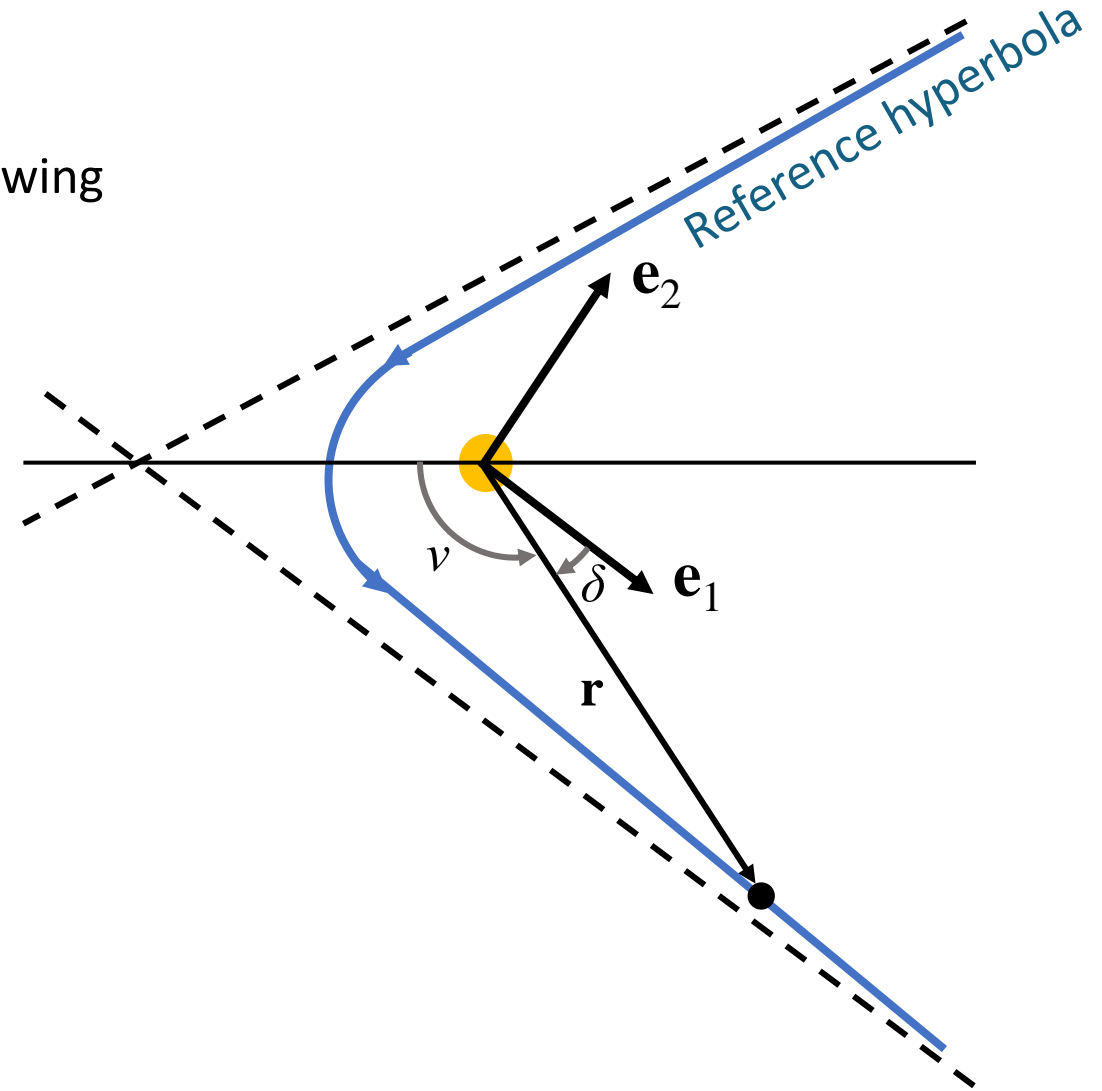
- ν – the chief's true anomaly

$$\nu \in (-\nu_{max}, \nu_{max}), \nu_{max} = \arccos\left(\frac{-1}{e}\right)$$

- $\delta := \nu_{max} - \nu$

$$\delta \in (0, 2\nu_{max}), \dot{\delta} < 0,$$

$$\delta \xrightarrow[t \rightarrow +\infty]{} 0, \delta = O\left(\frac{1}{r}\right)$$



SOLUTION OF THE LINEARIZED SYSTEM

Linearized system

$$\dot{\mathbf{x}} = \mathbf{A}(t) \mathbf{x}$$

$$\mathbf{x} := \begin{pmatrix} \boldsymbol{\rho} \\ \dot{\boldsymbol{\rho}} \end{pmatrix}, \Delta t := t - t_0$$

Solution

$$\mathbf{x}(t) = \mathbf{U}(t, t_0) \boldsymbol{\xi}$$

$\boldsymbol{\xi}$ is a vector of constants

Relates to the *initial conditions* via
 $\boldsymbol{\xi} = \mathbf{U}^{-1}(t_0, t_0) \mathbf{x}(t_0)$

We designate components

$$\boldsymbol{\xi} = (\alpha_{-1} \quad \alpha_0 \quad \beta_{-1} \quad \beta_0 \quad \gamma_{-1} \quad \gamma_0)^T$$

Note: $\boldsymbol{\xi}$ has units of distance (km)

$\mathbf{U}(t, t_0)$ is a *fundamental matrix*
 [Reynolds, 2022]:
 $\mathbf{U}(t, t_0) = \mathbf{U}(\mathbf{r}(t), \mathbf{v}(t), \Delta t)$

$$\mathbf{r} = \frac{a(e^2 - 1)}{1 - \cos \delta + \eta \sin \delta} \begin{pmatrix} \cos \delta \\ -\sin \delta \\ 0 \end{pmatrix}$$

$$\mathbf{U}(\mathbf{r}(\delta), \mathbf{v}(\delta), \Delta t(\delta, \delta_0))$$

$$\mathbf{v} = \frac{v_\infty}{\eta} \begin{pmatrix} \eta + \sin \delta \\ \cos \delta - 1 \\ 0 \end{pmatrix}$$

We use δ instead of time

Here $\eta := \sqrt{e^2 - 1}$

LAURENT SERIES EXPANSION

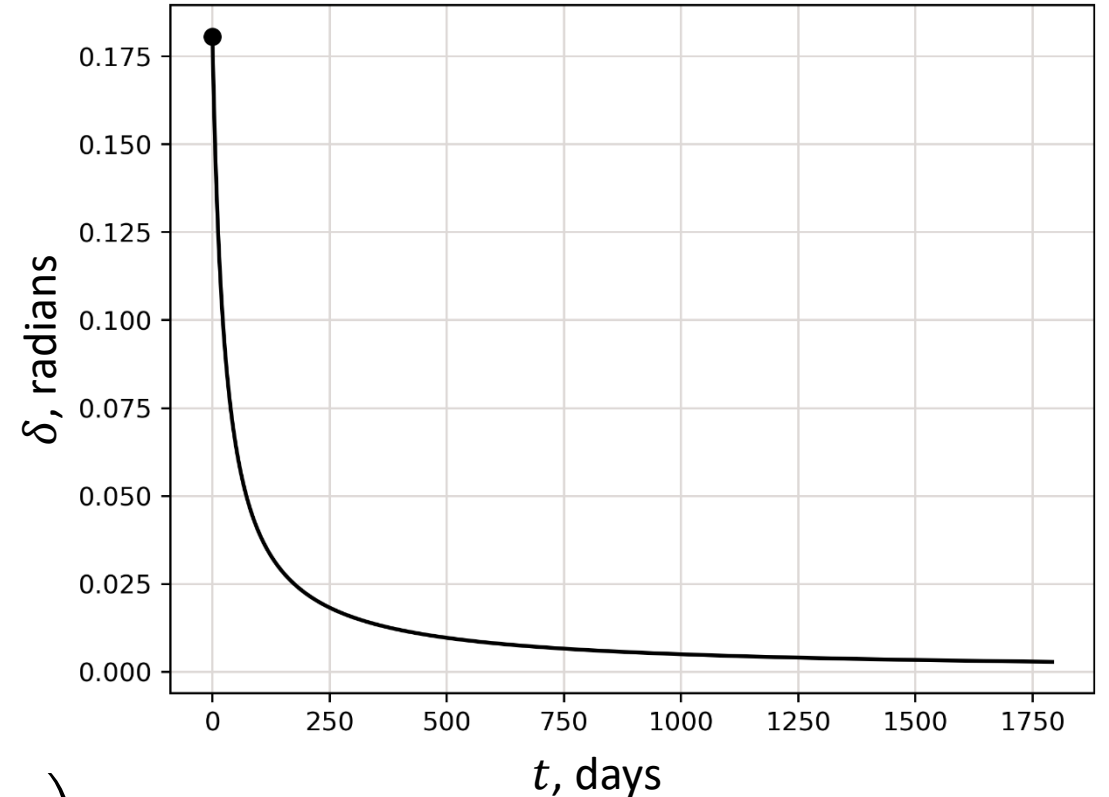
$\mathbf{U}(\mathbf{r}(\delta), \mathbf{v}(\delta), \Delta t(\delta, \delta_0))$ Let us exploit the natural asymptotic behavior: $\delta \rightarrow 0 +$

$$\mathbf{r} = \frac{\mu\eta}{v_\infty^2} \begin{pmatrix} \frac{1}{\delta} - \frac{1}{2\eta} + \left(-\frac{1}{3} + \frac{1}{4\eta^2}\right)\delta + O(\delta^2) \\ -1 + \frac{\delta}{2\eta} + O(\delta^2) \\ 0 \end{pmatrix}$$

$$\mathbf{v} = v_\infty \begin{pmatrix} 1 + \frac{\delta}{\eta} + O(\delta^3) \\ -\frac{\delta^2}{2\eta} + O(\delta^3) \\ 0 \end{pmatrix}$$

$$\Delta t(\delta, \delta_0) = \frac{\mu}{v_\infty^3} \left(\frac{\eta}{\delta} + \left(\frac{1}{2} - M_0\right) - \ln \frac{2\eta}{\delta e} - \frac{4\eta^2 + 9}{12\eta} \delta + O(\delta^2) \right)$$

$M_0 := e \sinh H(\delta_0) - H(\delta_0)$, H is the *hyperbolic anomaly*



Angle δ as a function of time

δ -EXPLICIT AND TIME-EXPLICIT ASYMPTOTIC SOLUTIONS

$$x(\delta) = \frac{\alpha_{-1}}{2\delta\eta} - \frac{3\alpha_{-1}}{2\eta^2} \ln \frac{2\eta}{\delta e} + \alpha_0 - \alpha_{-1} \left(\frac{6M_0 - 11}{4\eta^2} \right) + O(\delta \ln \delta),$$

$$y(\delta) = \frac{\beta_{-1}}{\delta} + \beta_0 + \frac{\alpha_{-1}}{\eta} - \left(\frac{\beta_{-1}}{3} + \frac{\beta_0}{2\eta} + \frac{5\alpha_{-1}}{4\eta^2} \right) \delta + o(\delta),$$

$$z(\delta) = \frac{\gamma_{-1}}{\delta} + \gamma_0 - \left(\frac{\gamma_{-1}}{3} + \frac{\gamma_0}{2\eta} \right) \delta + o(\delta).$$

Note:

$\alpha_{-1}, \beta_{-1}, \gamma_{-1}$ are first met with δ^{-1}
 $\alpha_0, \beta_0, \gamma_0$ are first met with δ^0

δ -explicit
 asymptotic solution

$$\delta = \eta \frac{1}{\tau_\pi} - \eta \frac{\ln \tau_\pi}{\tau_\pi^2} + \eta \left(\frac{1}{2} + \ln \frac{e}{2} \right) \frac{1}{\tau_\pi^2} + o\left(\frac{1}{\tau_\pi^2}\right), \quad \tau_\pi \rightarrow +\infty, \quad \text{where } \tau_\pi := \frac{v_\infty^3}{\mu} (t - \tau)$$

$$x(\tau_\pi) = \frac{\alpha_{-1}}{2\eta^2} \tau_\pi - \frac{\alpha_{-1}}{\eta^2} \ln \left(\frac{2}{e} \tau_\pi \right) + \alpha_0 + \alpha_{-1} \left(\frac{5}{2\eta^2} - \frac{3M_0}{2\eta^2} \right) + O\left(\frac{\ln \tau_\pi}{\tau_\pi}\right),$$

$$y(\tau_\pi) = \frac{\beta_{-1}}{\eta} \tau_\pi + \frac{\beta_{-1}}{\eta} \ln \left(\frac{2}{e} \tau_\pi \right) + \beta_0 + \frac{2\alpha_{-1} - \beta_{-1}}{2\eta} + O\left(\frac{\ln \tau_\pi}{\tau_\pi}\right),$$

$$z(\tau_\pi) = \frac{\gamma_{-1}}{\eta} \tau_\pi + \frac{\gamma_{-1}}{\eta} \ln \left(\frac{2}{e} \tau_\pi \right) + \gamma_0 - \frac{\gamma_{-1}}{2\eta} + O\left(\frac{\ln \tau_\pi}{\tau_\pi}\right).$$

Time-explicit
 asymptotic solution

POSSIBLE TYPES OF HYPERBOLIC RELATIVE MOTION

1. The relative motion is bounded if and only if

$\alpha_{-1} = \beta_{-1} = \gamma_{-1} = 0$,
otherwise it is unbounded

Note:

These conditions are equal to three
linear equations on the initial state $\mathbf{x}(t_0)$
(initial relative velocity ≈ 0)

2. If the motion is bounded, the relative trajectory
is generally a line segment

(if $\alpha_0, \beta_0, \gamma_0 \neq 0$, then $(x, y, z)^T$ tends to $(\alpha_0, \beta_0, \gamma_0)^T$)

- If at least one of $\alpha_0, \beta_0, \gamma_0$ is zero, the geometry is more complicated
(for example, it can be a segment of parabola in certain 2D projections)

3. If the motion is unbounded, the relative trajectory
is generally an infinite ray

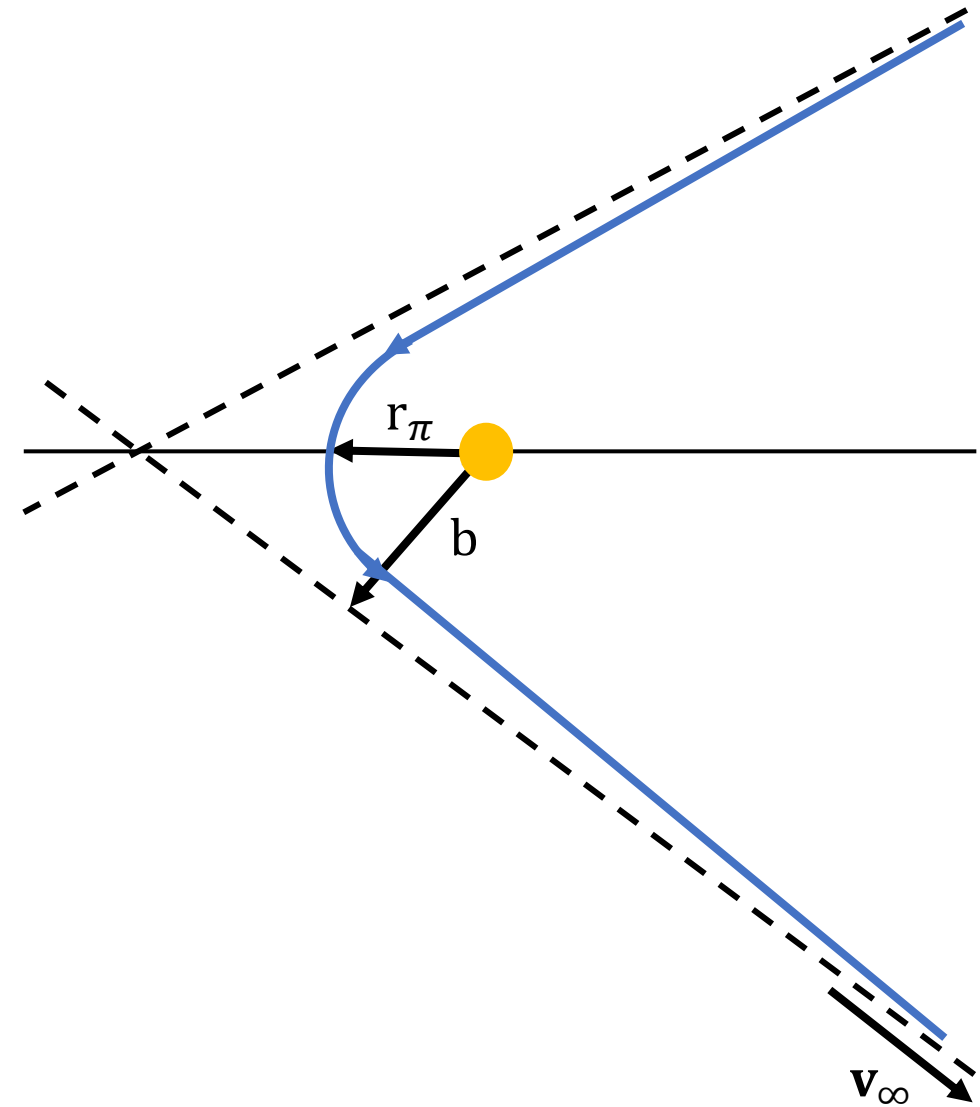
$(x = \frac{\alpha_{-1}}{2\eta^2} \tau_\pi + o(\tau_\pi), y = \frac{\beta_{-1}}{\eta} \tau_\pi + o(\tau_\pi), z = \frac{\gamma_{-1}}{\eta} \tau_\pi + o(\tau_\pi))$

- If at least one of $\alpha_{-1}, \beta_{-1}, \gamma_{-1}$ is zero, the geometry is more complicated
(for example, it can be a hyperbola in certain 2D projections)

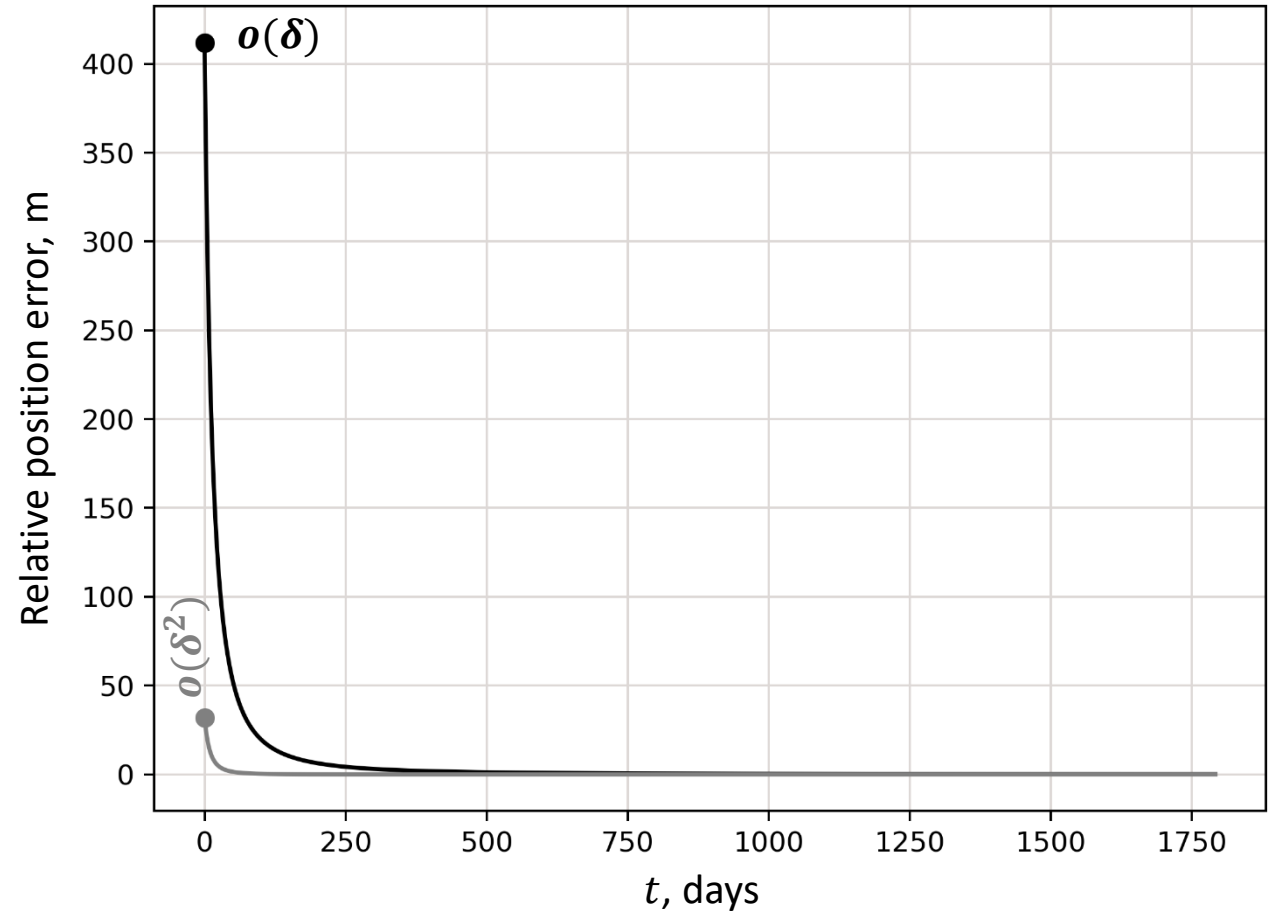
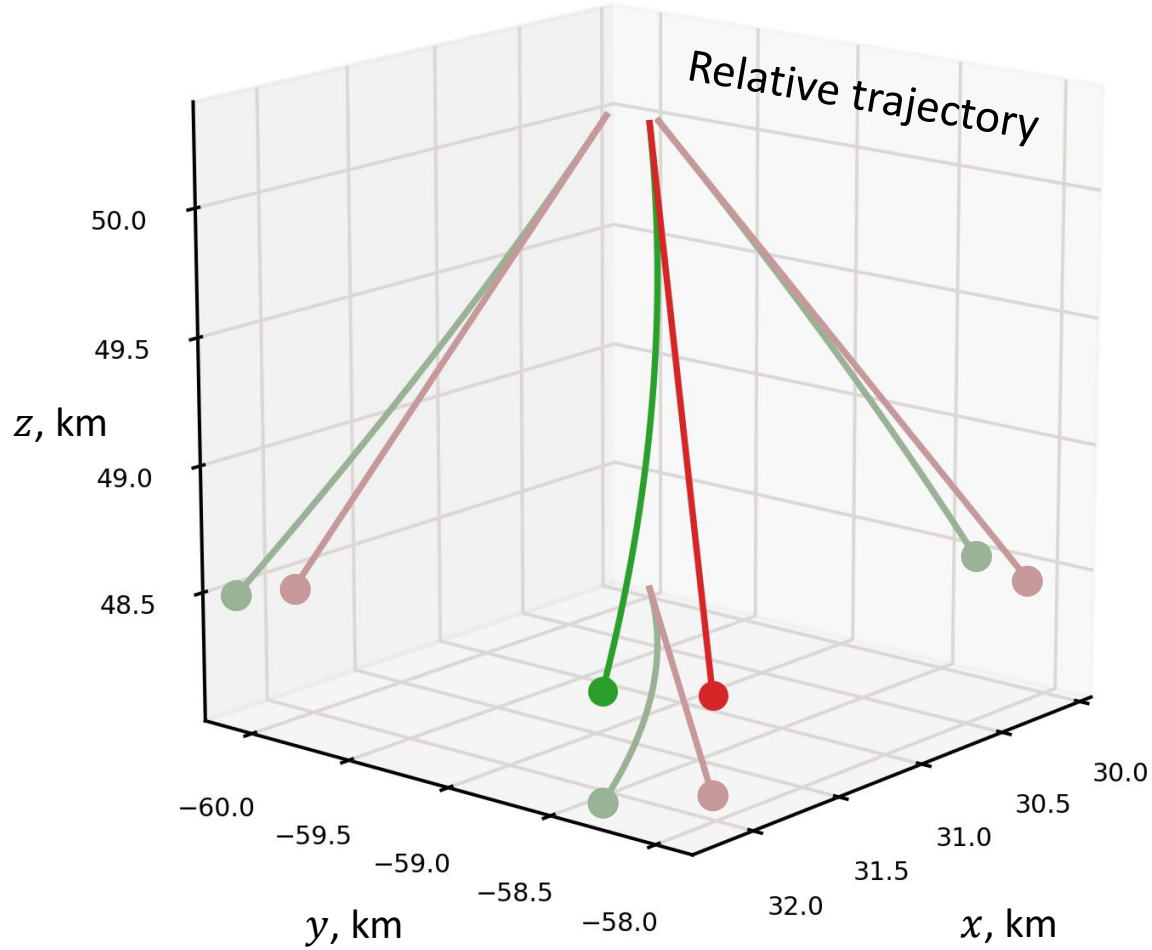
The hyperbolic case is much
poorer in types of relative motion
than the elliptic/circular case

THE REFERENCE TRAJECTORY

- Heliocentric
- Hyperbolic excess velocity $v_{\infty} = 20 \frac{\text{AU}}{\text{year}} \approx 95 \frac{\text{km}}{\text{s}}$
- Eccentricity $e \approx 3.03$
- Impact parameter $b = 0.28 \text{ AU}$
- Pericenter distance $r_{\pi} = 0.20 \text{ AU}$
- Semi-major axis $a = 0.10 \text{ AU}$
- Initial chief's position $r_0 = 1.52 \text{ AU}$ ($\delta_0 \approx 0.1807$)
- Final chief's position $r_f = 100 \text{ AU}$ ($\delta_f \approx 0.0028$)



EXAMPLE: BOUNDED MOTION



Unperturbed 2-body
problem solution

First-order
asymptotic solution

$$\alpha_{-1} = \beta_{-1} = \gamma_{-1} = 0$$

$$\alpha_0 = 30 \text{ km}$$

$$\beta_0 = -60 \text{ km}$$

$$\gamma_0 = 50 \text{ km}$$

$$x(\delta) = \alpha_0 \left(1 + \frac{\delta}{\eta}\right), \quad y(\delta) = \beta_0 \left(1 - \frac{\delta}{2\eta}\right), \quad z(\delta) = \gamma_0 \left(1 - \frac{\delta}{2\eta}\right)$$

Error $|\mathbf{p}_{exact} - \mathbf{p}_{approx}|$ between exact (2BP)
and first/second-order approximate solutions

EXAMPLE: REGULAR TETRAHEDRON FORMATION

Since the motion is bounded, for all deputies

$$\alpha_{-1} = \beta_{-1} = \gamma_{-1} = 0$$

Recalling that $(x, y, z)^T$ tends to $(\alpha_0, \beta_0, \gamma_0)^T$, it is easy to find

$$\xi_1 = \left(0 \quad -\frac{\sqrt{6}}{3}l \quad 0 \quad -\frac{1}{2}l \quad 0 \quad -\frac{1}{2\sqrt{3}}l \right)^T$$

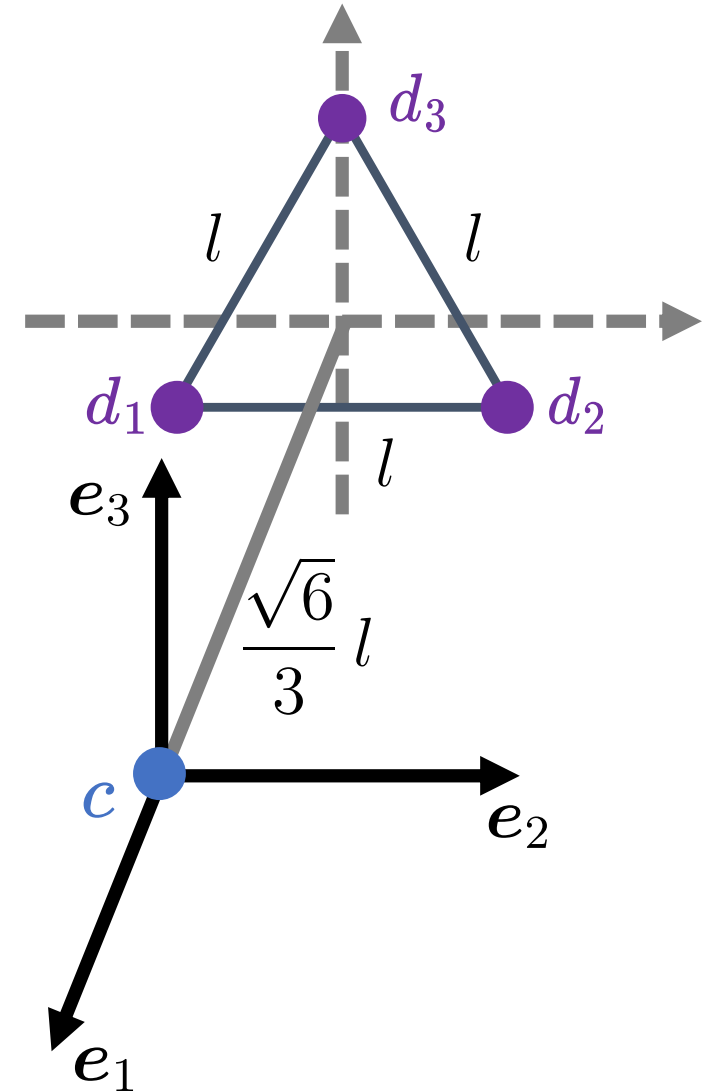
$$\xi_2 = \left(0 \quad -\frac{\sqrt{6}}{3}l \quad 0 \quad \frac{1}{2}l \quad 0 \quad -\frac{1}{2\sqrt{3}}l \right)^T$$

$$\xi_3 = \left(0 \quad -\frac{\sqrt{6}}{3}l \quad 0 \quad 0 \quad 0 \quad \frac{1}{\sqrt{3}}l \right)^T$$

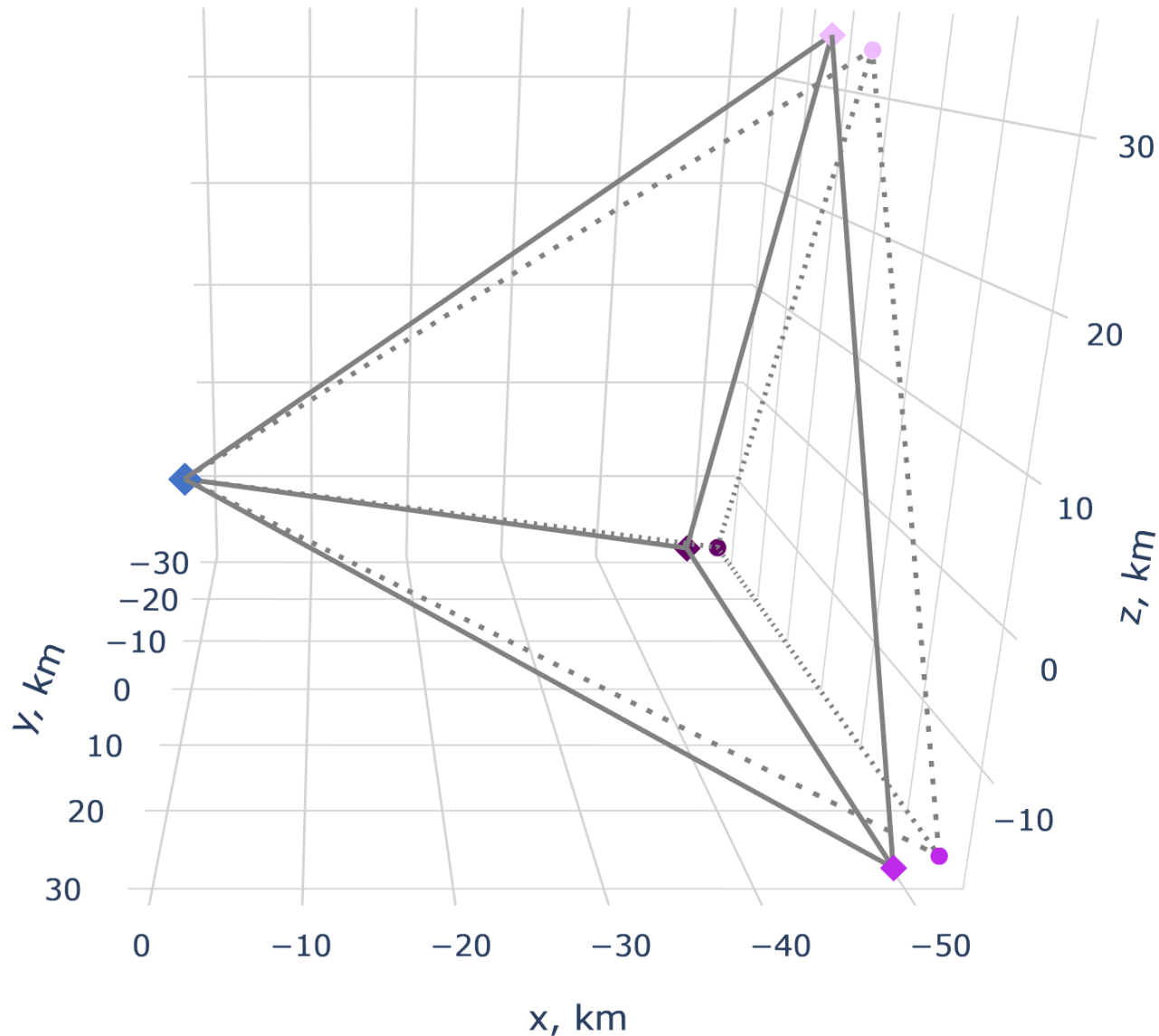
Convert into initial relative position & velocity

$$\rho_1(t_0) = l \text{ [km]} \cdot (-0.87 \text{ km} \quad -0.48 \text{ km} \quad -0.28 \text{ km})^T$$

$$\dot{\rho}_1(t_0) = l \text{ [km]} \cdot \left(0.019 \frac{\text{mm}}{\text{s}} \quad -0.010 \frac{\text{mm}}{\text{s}} \quad -0.004 \frac{\text{mm}}{\text{s}} \right)^T$$



EXAMPLE: REGULAR TETRAHEDRON FORMATION SIMULATION



Evolution of a tetrahedron with $l = 60 \text{ km}$
from the epoch at $r = 1.52 \text{ AU}$
to the epoch at $r = 100 \text{ AU}$

Dashed lines – tetrahedron at the initial epoch
Solid lines – tetrahedron at the final epoch

Simulation was done numerically
in the unperturbed 2-body problem
with initial conditions calculated analytically

During all the flight time, the tetrahedron
was almost regular with the required size

No control or correction was applied!

CONCLUSION

- A new asymptotic representation for describing relative motion between spacecraft in hyperbolic trajectories is developed
 - Time-explicit formulae are obtained
- Based on the representation, possible types of relative motion are classified
 - Hyperbolic case turns out to be quite poor in terms of types compared to elliptic/circular case
- A way to design a spacecraft formation using the representation is proposed and demonstrated by the regular tetrahedron example
- Areas of application:
control & navigation problems solution;
formation deployment and maintenance;